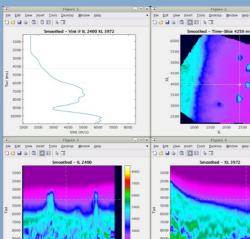
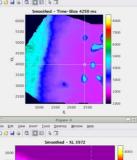


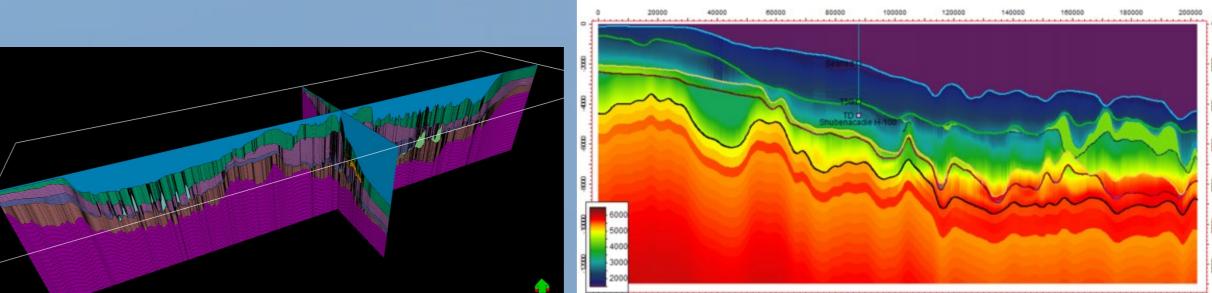
# BeicipFranlab

# Nova Scotia Offshore Velocity Modeling 2022

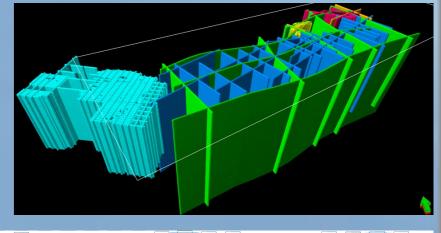


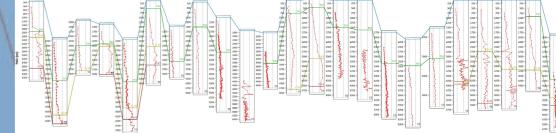




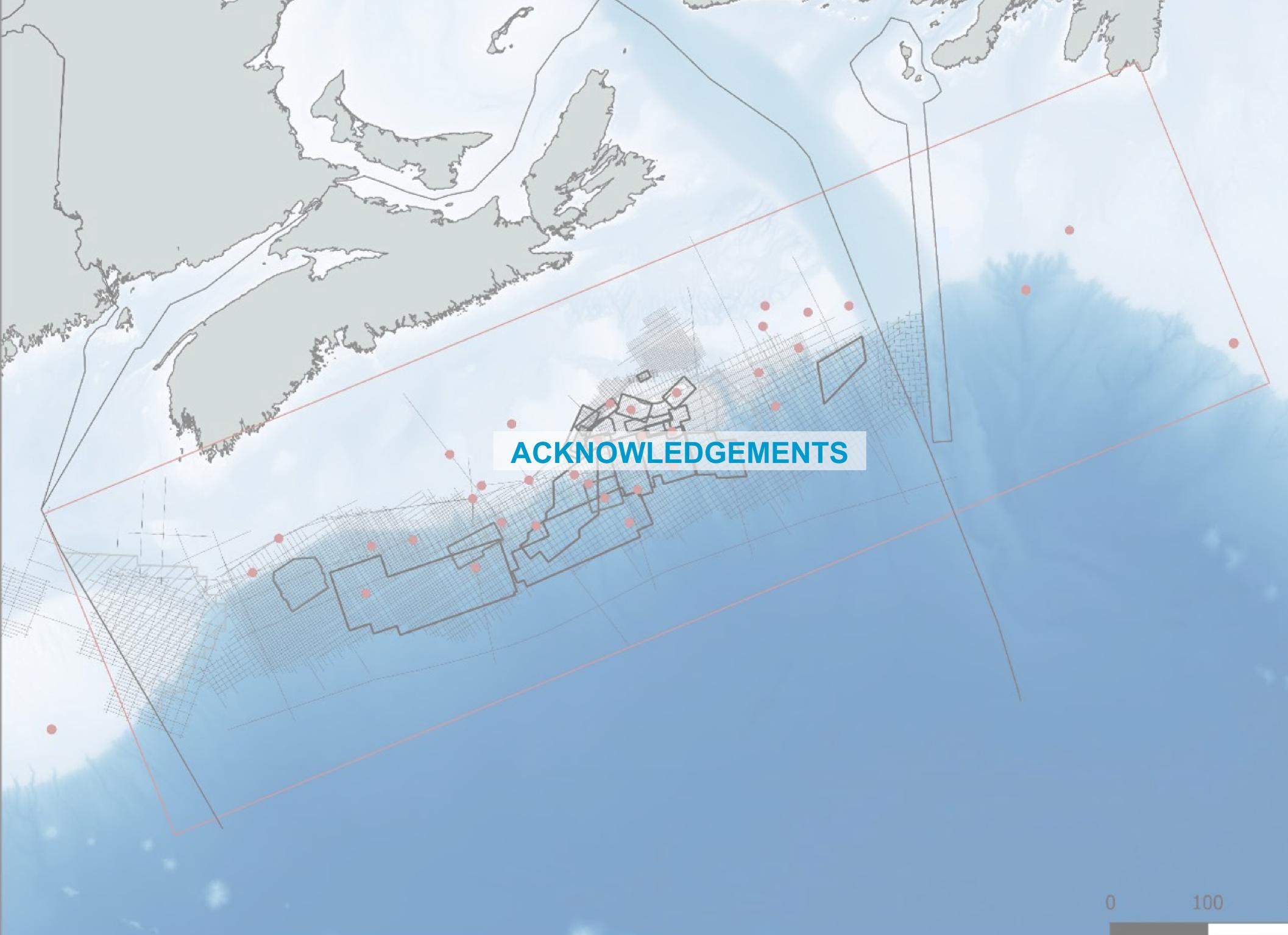








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### **Offshore Nova Scotia Velocity Modeling – CANADA – January 2022**

Offshore Nova Scotia Velocity Modeling – CANADA – January 2022

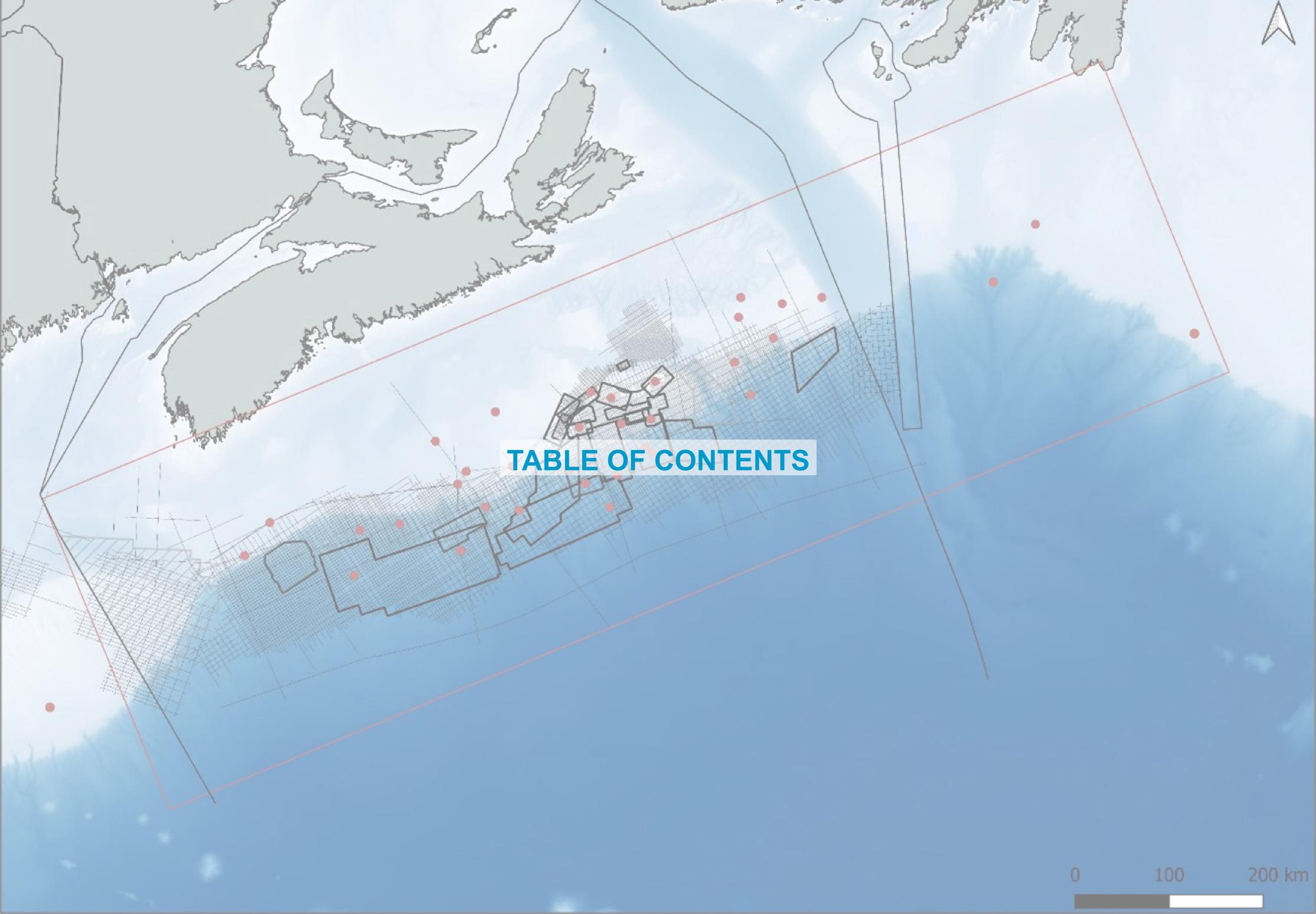
### ACKNOWLEDGEMENTS:

This project relies on contributions from many individuals from a variety of disciplines and organizations that are listed below.



# BeicipFranlab

Organisation	Contributors
cotia Department of Natural ces and Renewables	Fraser Duncan Keppie, Adam MacDonald, Natasha Morrison
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ranlab	Ingrid Breda-Dupin, Tomasz Chrest, Laurent Cuilhe



### **OFFSHORE NOVA SCOTIA VELOCITY MODELING**

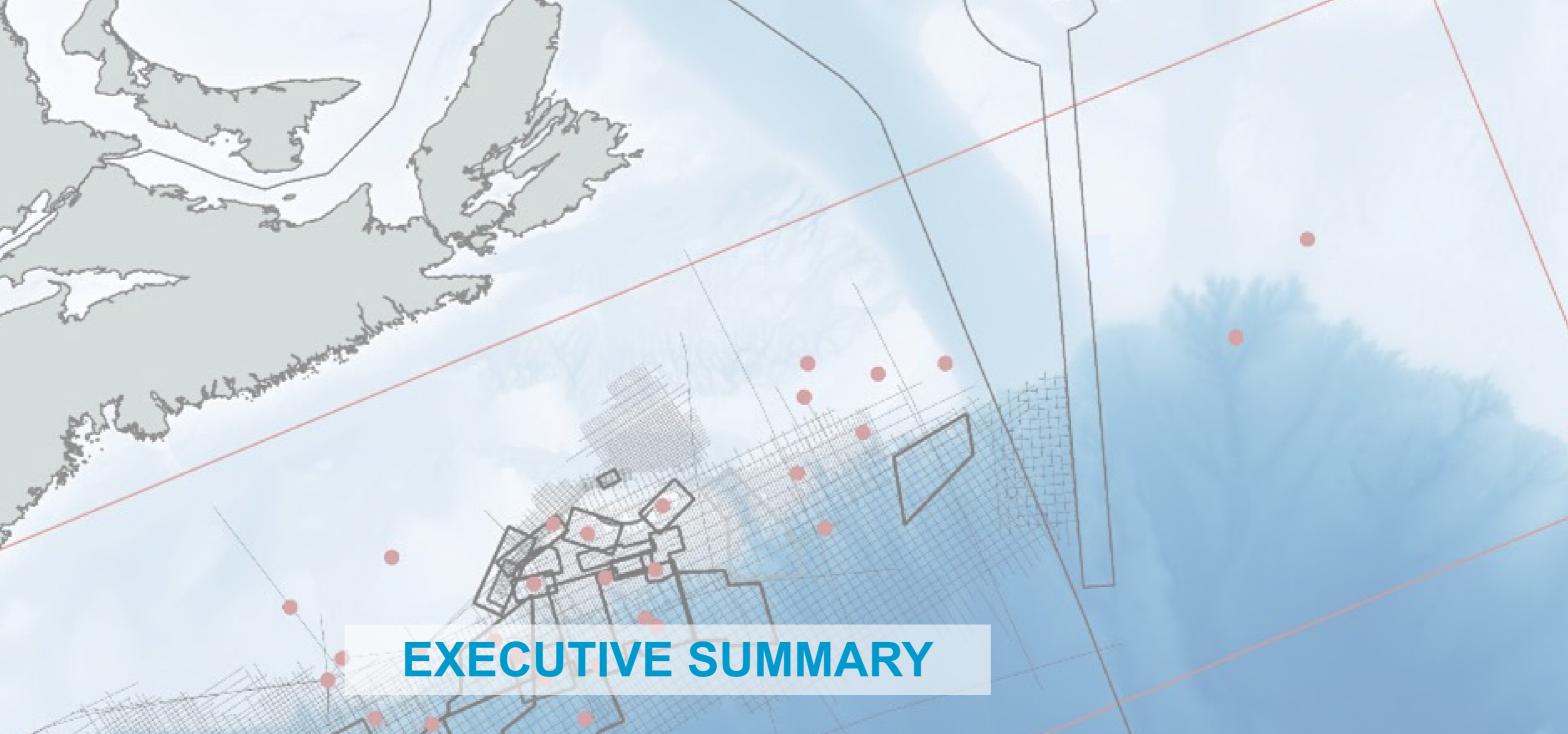
**OFFSHORE NOVA SCOTIA VELOCITY MODELING - CANADA – January 2022** 

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Strate to Barriel

### **Executive Summary**

### Introduction – Objectives

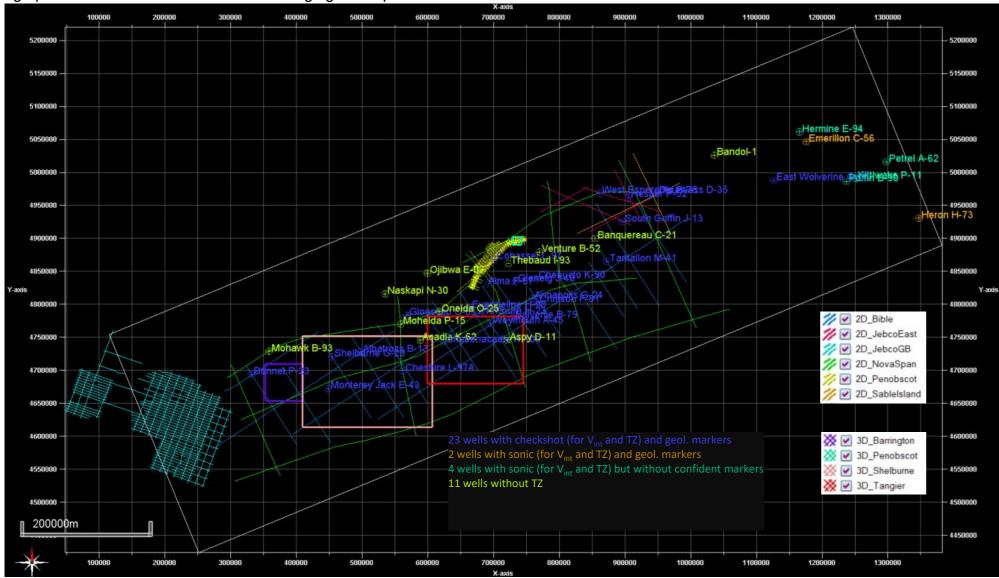
In past Play Fairway Analysis (PFA) projects 2010-2021, velocity models were variously developed to allow time-to-depth conversion of interpreted seismic. In 2021, OERA / NSDRR (previously NSDEM) find themselves with a collection of past PFA regions of interest with different stages of interpretation and velocity models.

CNSOPB and others have updated interpretations of some horizons in time for different parts of the margin. To make use of these past projects and new updates in the depth domain, OERA / NSDRR are faced with the general challenge of creating and justifying a time-to-depth or velocity model conversion.

This study provides OERA / NSDRR with a regional time-to-depth velocity model that integrates diverse inputs and reconciles inconsistencies in a systematic way to support approximate, yet reasonable depth-converted seismic interpretations with justification in offshore Nova Scotia.

### Database

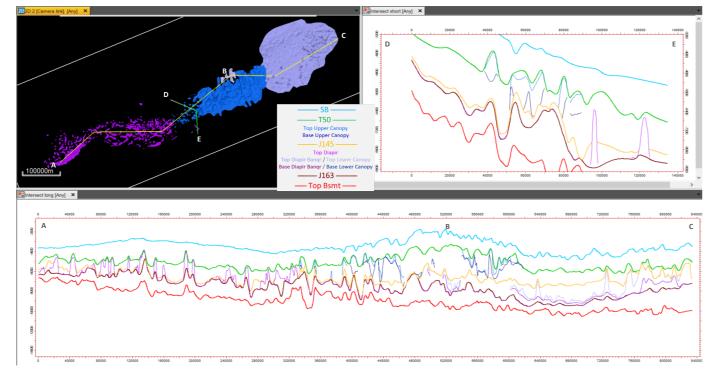
A rectangular area – the AOI – delimits the zone where the velocity model is constructed. It measures 358 x 1224 km along a WSW-ENE main direction (structurally the main N68 'strike' direction), delimiting a 438,000 km<sup>2</sup> surface, and covers the whole offshore Nova Scotian margin plus a large part of the Laurentian sub-basin belonging to the province of Newfoundland and Labrador.



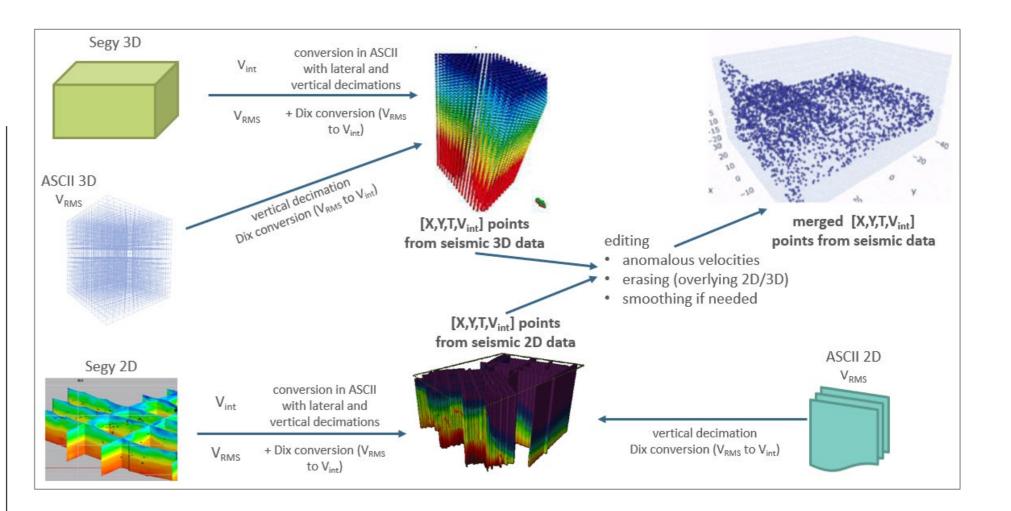
A total of 40 wells are considered, whatsoever about the type of data they include (checkshot or VSP data, sonic log, geological markers).

Seismic processing velocities of any kind are divided into six 2D surveys and four 3D cubes.

The AOI encompass five gridded main horizons. Three sets of salt horizons divide the salt area into diapirs and canopies. They were smartly worked to get extended horizons that do not cross each other.



### **Executive summary**

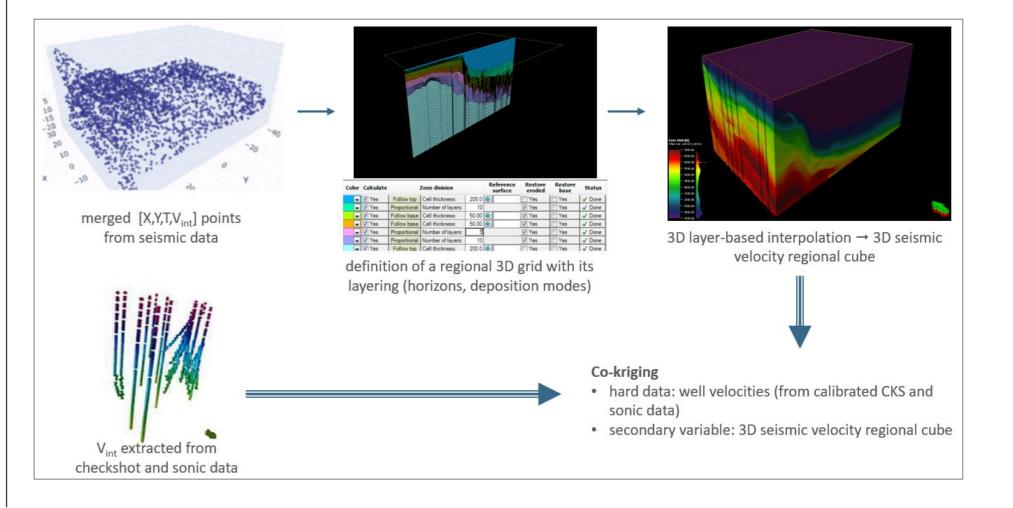


### Methodology

Phase 1 (top): Creation of a merged set of [X,Y,T,V<sub>int</sub>] points from various sources of raw seismic velocities. Different kind of editing (erasing, cropping, smoothing, upscaling) were done before merging.

Phase 2 (bottom): 3D interpolation of seismic velocities through a stratigraphic model built using all the horizons after editing them. Different zones of layering are set between the edited horizons: regular layering in the sedimentary/reservoir zones, constant layer/velocity in the salt and water.

Phase 3 (bottom): Co-kriging of the calibrated well velocities with the seismic velocity cube. Such co-kriging preserves the calibrated TZ laws, consequently no further residual correction would be necessary (the residuals are corrected/estimated previously to the cokriging).



### **Executive Summary**

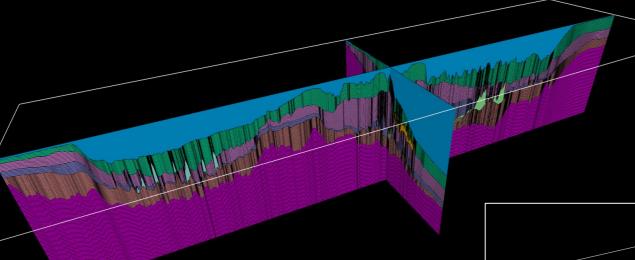
### Calibrating the well velocities

Specific workflows were created to set the well velocities to an optimal vertical calibration (from depth to time), whether with the checkshot velocities or the sonic ones. After a first estimation, the TZ calibrations were corrected using the horizons/markers match, without forcing the checkshot velocities (correction done 'at best' with all the relevant markers/horizons couples). Some easternmost wells in the Laurentian sub-basin have too much uncertainties in their markers depth values to be processed with the same recalibration: their digitized sonic logs were set with a simple calibration (TZ from the extrapolated sonic).

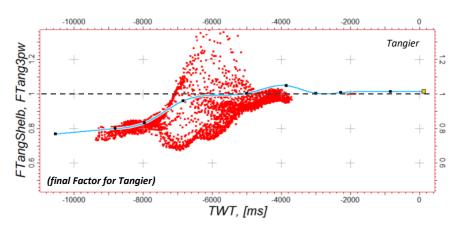
Some checkshot velocities were completed – using seismic velocity trends – in the parts where data was missing.

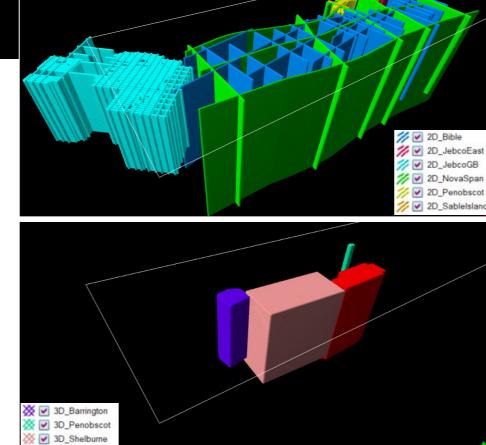
### Seismic Velocity interpolation

A single blank 3D TWT grid was created within the AOI with a lateral mesh of 1 x 1 km, and a vertical layering of 50 ms in the reservoir zones, as illustrated here below.



The [X,Y,T,V<sub>int</sub>] points were upscaled into the grid, as illustrated to the right. It enabled to compute ratio factors between well, 2D and 3D velocities, and adjust the different seismic velocity sources at best, especially between adjacent velocity cubes. An example of ratio factor here below illustrates how the interval velocities were modified in that cube following the depth (TWT here), in order to accommodate the values with other sources.





Various editing passes were also needed for 2D and 3D velocities (with the addition of some pseudo-traces to control the extrapolation). A Moving Average interpolator enabled to fill the whole 3D grid, which represents the "trend" for the following co-kriging.

### Co-kriging

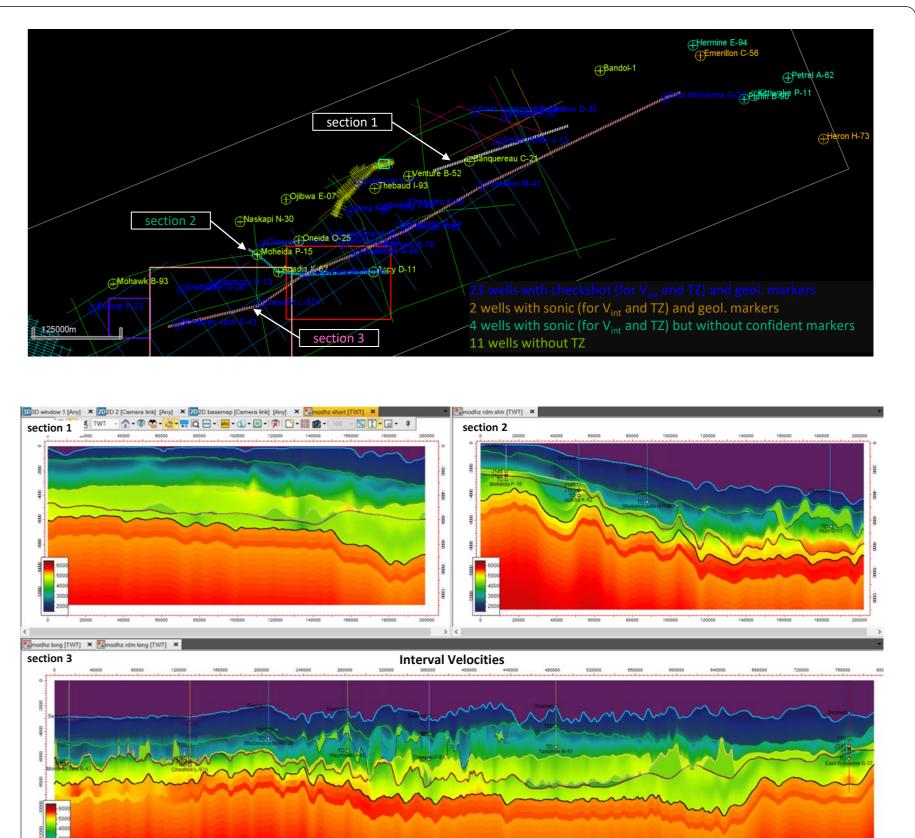
The calibrated well velocities (hard data) were co-kriged using the seismic velocity property as secondary variable. Constant velocity layers were filled separately. After a first pass, the resulting velocities were extracted at the 11 wells without own TZ, to get their first Depth to Time conversion that was afterwards adjusted with the help of the markers/horizons couples. A second and definitive co-kriging was then run with all the wells. The figures on the right illustrate 3 sections with the cokriged interval velocity and the resulting average velocity (used for conversions).

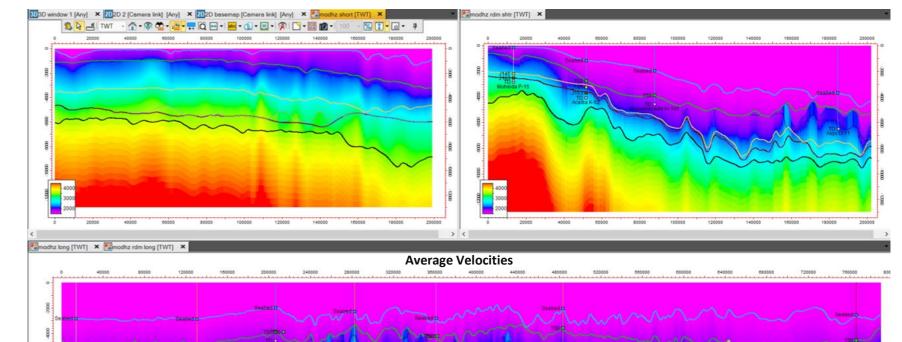
💥 🗹 3D\_Tangier

### Conclusion

To reach the objectives of the project, all the sources of available velocities (3D and 2D seismic data, checkshot, sonic, constant velocity in the salt) were used. They were worked to their optimal possibility, especially the large adjacent 3D sets were adjusted between them and with the true well velocities. The geological markers and the time horizons were jointly compared to calibrate the raw velocities (checkshot or sonic) at the wells  $\rightarrow$  the final model respects that calibration. Limitations : some 2D seismic velocity sets remain different between themselves in the deep layers (below the total depth of the wells), without the possibility to identify where is the best accuracy; the Velocity Model is more uncertain far from the wells – especially the 11 ones without own TZ – and in the deeper interval below J145 poorly drilled by the wells and with a low Signal / Noise ratio leading to more uncertain seismic processing velocities ; this Velocity Model does not consider any local geological feature, not identified with the current input data, as a source of local velocity anomaly.

The Average Velocity property is now implemented into a Petrel<sup>TM</sup> Velocity Model.





# CHAPTER 1

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# DATABASE CONSTRUCTION FOR VELOCITY MODELING

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### Area of Interest (AOI)

[NB: the geodetical datum used in this project and in the figures is NAD-1927; the cartographic projection is UTM 20N]

A rectangular area (Figure 1) delimits the zone where the velocity model is constructed. It measures 358 x 1224 km along a WSW-ENE main direction (structurally the main N68 'strike' direction), delimiting a 438,000 km<sup>2</sup> surface, and covers the whole offshore Nova Scotian margin plus a large part of the Laurentian sub-basin mainly located in the province of Newfoundland and Labrador.

The Figure 2 reminds the chronostratigraphic chart and underlines the stratigraphic location of the main time horizons with their names highlighted by red rectangles (see them in PL.1.3).

#### Wells

A total of 40 wells are taken into account, whatsoever about the type of data they include (checkshot or VSP data, sonic log, geological markers). A detailed list of them is added in PL. 1.2. They may be divided into 4 groups:

- 23 wells with checkshot data and geological markers (in blue in Figure 1)
- 2 wells with sonic log and geological markers (in orange)
- 4 wells with sonic log, with no geological markers except some litho-stratigraphical information (in dark green)
- 11 wells without TZ (Time-to-Depth) data (in light green)

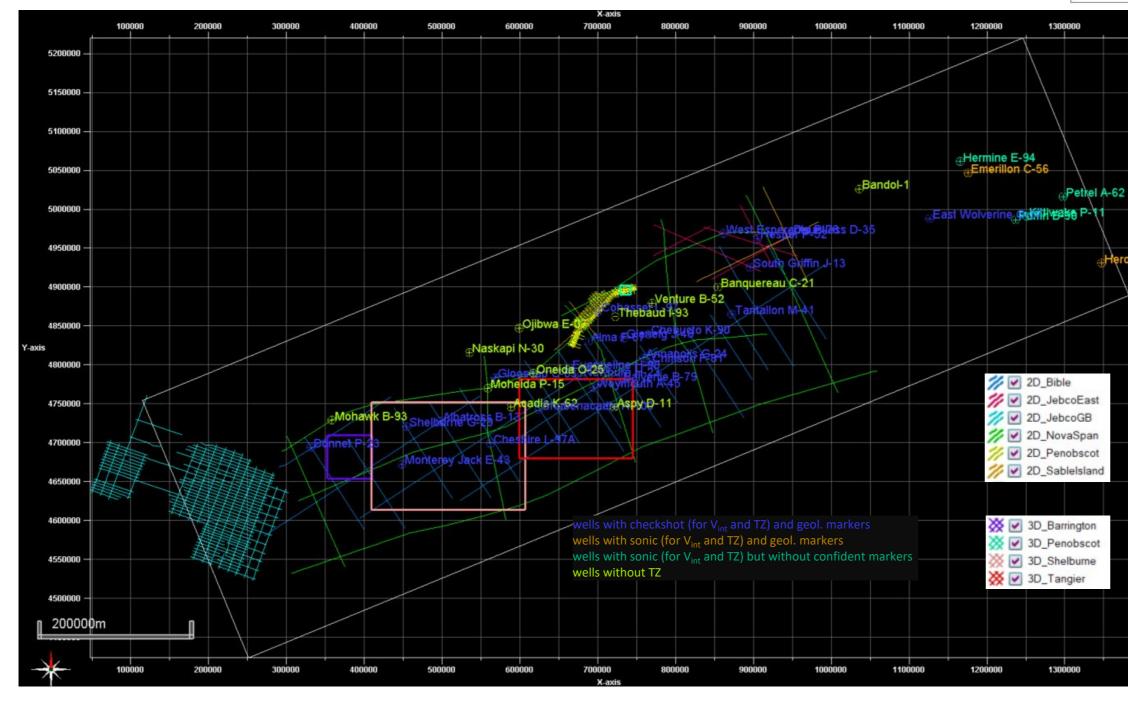


Figure 1: Basemap and AOI (Area Of Interest) limits

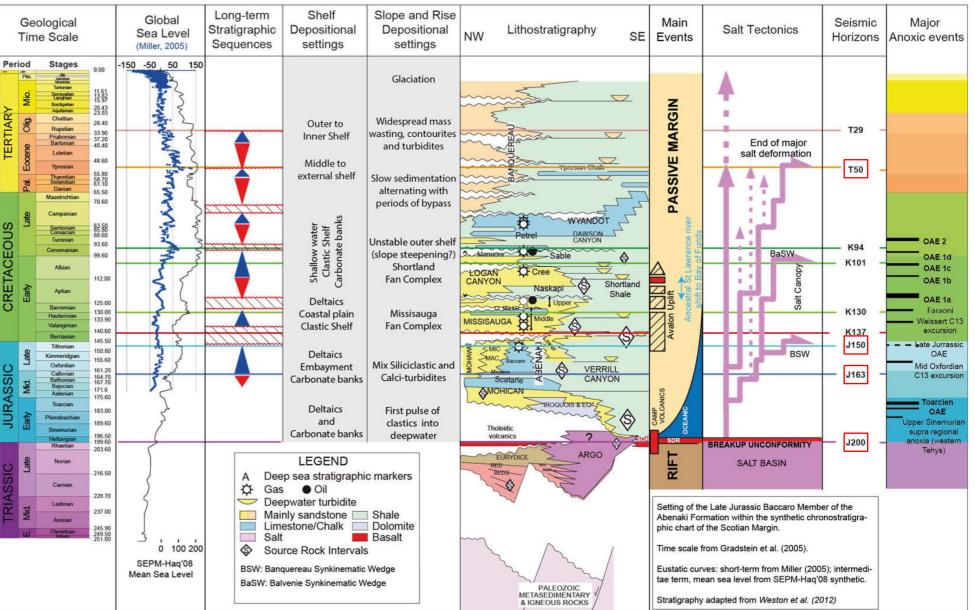


Figure 2: Chronostratigraphic chart of Nova Scotian margin

#### Seismic velocity data

Different types of seismic velocities (more precisely seismic processing velocities) are used, with their respective velocity properties, vertical sampling and file format. A detailed list of them is available in PL. 1.3. They are available into 3D surveys (4 cubes) and 2D surveys (6 sets): their locations are displayed here to the left. In the last eastern quarter of the AOI (Laurentian Basin), no seismic velocity is provided.

Most of the 3D surveys are adjacent and located in the main Shelburne basin:

- Barrington (~ 2300 km<sup>2</sup>)
- Shelburne (~ 15300 km<sup>2</sup>)
- Tangier (~ 8300 km<sup>2</sup>)

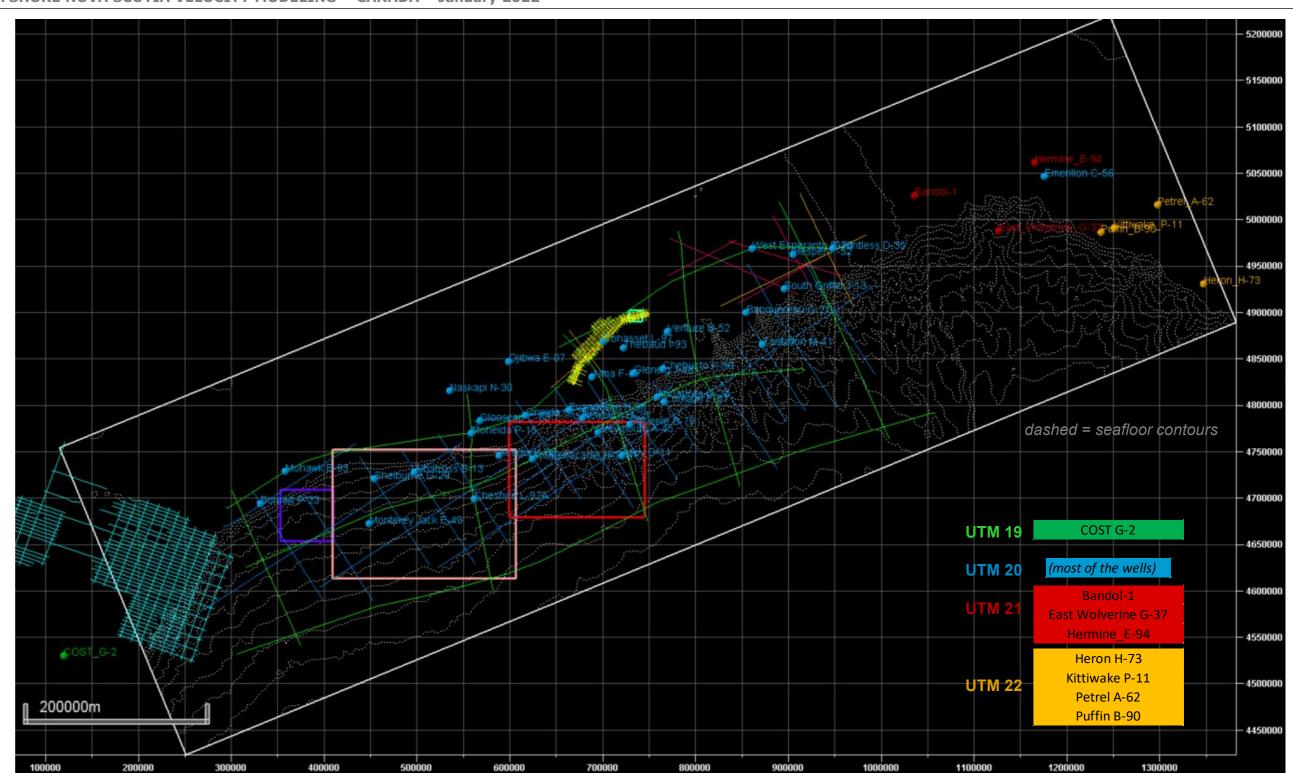
The last 3D survey – Penobscot – is much smaller (~ 90 km<sup>2</sup>) and located to the North of Thebaud I-93 well.

The 6 surveys of 2D lines are better distributed in the whole Nova Scotian margin. A detailed list of them is presented in PL. 1.4. The 6 surveys are:

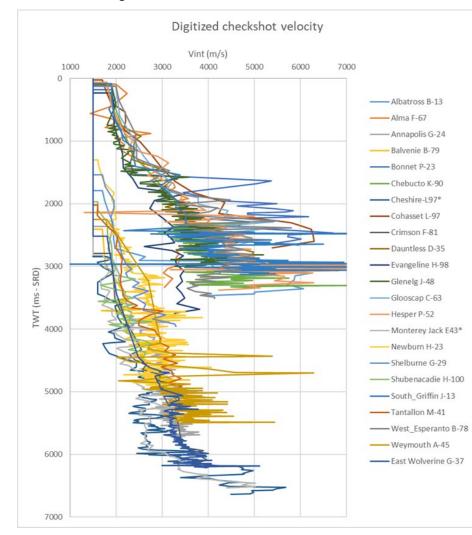
- Bible: long lines covering the whole Nova Scotian margin
- Jebco East: some lines in the northern area, around West-Esperanto B-78
- Jebco Georges Bank: dense set of lines covering the extreme western part of the AOI
- Nova Span: as Bible set, with a denser coverage
- Penobscot: very dense set of short lines localised in a small area around Cohasset L-97
- Sable Island: few lines (2 in Penobscot survey and 2 in among Jebco East survey)

Well	dev'd	deviation	CKS vel.	Sonic log	no TZ	no geol. mark.	Х	Y	UTM	RT
40	18		23	6	11	4				
-		<b>•</b>	-		· •	<b>v</b>	-	•		
Acadia K-62		dif.TD 2 m			x		588433	4745831	UTM 20	13
Albatross B-13		vertical	x				496994	4727585	UTM 20	24
Alma F-67	D	dif.TD 11 m	x				688407	4830393	UTM 20	24
Annapolis G-24	D	dif.TD 26 m	x				758531	4808827	UTM 20	36
Aspy D-11	D	dif.TD 206 m			x		720856	4745645	UTM 20	31
Balvenie B-79		vertical	x				729168	4779300	UTM 20	25
Bandol-1		no survey			x		564665	5003662	UTM 21	23
Banquereau C-21		dif.TD 1 m			x		854441	4899949	UTM 20	27
Bonnet P-23	D	dif.TD 10 m	х				331182	4693790	UTM 20	25
Chebucto K-90	D	dif.TD 8 m	х				764910	4839385	UTM 20	23
Cheshire L-97A	D	dif.TD 3 m	х				561754	4699121	UTM 20	32
Cohasset L-97	D	dif.TD 4 m	х				700665	4868393	UTM 20	33
Crimson F-81	D	dif.TD 68 m	х				766226	4803559	UTM 20	21
Dauntless D-35		no survey	х				947661	4968885	UTM 20	31
East Wolverine G-37	D	dif.TD 5 m	х				651698	4959297	UTM 21	32
Emerillon C-56	D	dif.TD 5 m		x			1175776	5046818	UTM 20	30
Evangeline H-98	D	dif.TD 11 m	х				663802	4794849	UTM 20	21
Glenelg J-48	D	dif.TD 13 m	х				733404	4834320	UTM 20	24
Glooscap C-63	D	dif.TD 15 m	х				567773	4783412	UTM 20	23
Hermine E-94		no survey		x		x	695812	5029266	UTM 21	26
Heron H-73		no survey		x			385591	4877173	UTM 22	26
Hesper P-52	D	dif.TD 3 m	x				905198	4962293	UTM 20	41
Kittiwake P-11		no survey		x		x	299537	4950343	UTM 22	26
Mohawk B-93		no survey			x		358193	4729045	UTM 20	31
Moheida P-15		no survey			x		558704	4769952	UTM 20	30
Monterey Jack E-43		dif.TD 1 m	x				448404	4672464	UTM 20	32
Naskapi N-30		vertical			x		535021	4815742	UTM 20	26
Newburn H-23	D	dif.TD 88 m	x				678317	4785626	UTM 20	24
Ojibwa E-07		no survey			x		599015	4847058	UTM 20	30
Oneida O-25		vertical			X		616903	4789243	UTM 20	26
Petrel A-62		no survey		x		x	349521	4968029	UTM 22	30
Puffin B-90		no survey		x		x	285289	4947815	UTM 22	30
Shelburne G-29		no survey	x				454159	4720817	UTM 20	25
Shubenacadie H-100		dif.TD 1 m	x				624365	4742186	UTM 20	24
South Griffin J-13		dif.TD 1 m	x				895795	4925546	UTM 20	40
Tantallon M-41		dif.TD 2 m	x				871906	4865251	UTM 20	24
Thebaud I-93	D	dif.TD 7 m			x		722474	4861934	UTM 20	3
Venture B-52	-	dif.TD 2 m			x		769669	4879374	UTM 20	34
West Esperanto B-78	D	dif.TD 3 m	x		^		861040	4968862	UTM 20	23
Weymouth A-45	D	dif.TD 20 m	x				695037	4770820	UTM 20	25

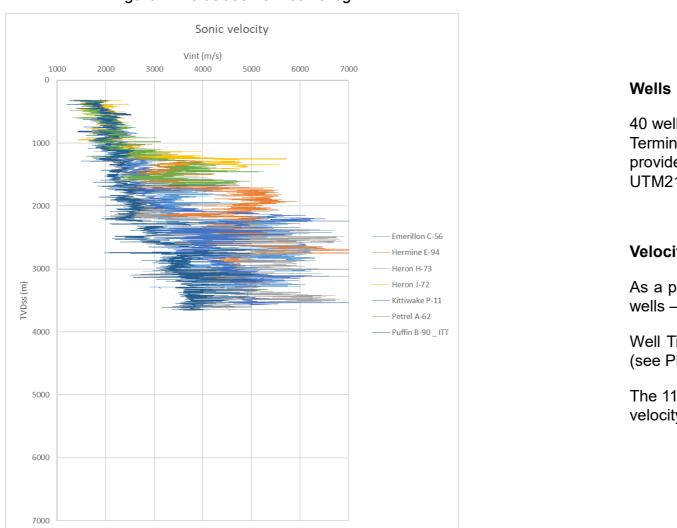
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### Figure 3: Velocities from checkshot data



### Figure 4: Velocities from sonic log



### Well velocities

Figure 2: Well basemap according to the original coordinate zones

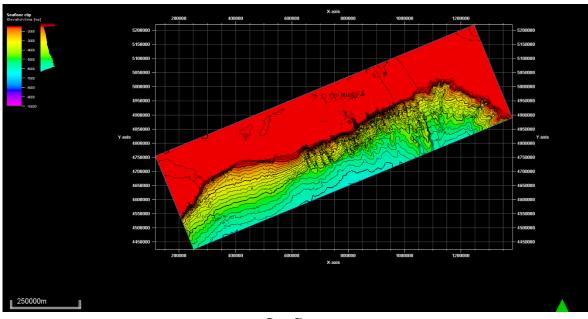
40 wells are available. Few of them are much deviated (Fig.1): only those whose depth difference TVD vs. MD at Terminal Depth is more than 3 m are considered as deviated with their deviation survey loaded into software. The provided coordinates are mainly UTM 20N (blue in Fig.2); the wells in the Laurentian sub-basin are provided in UTM21N or -22N.

### Velocity and TZ sources

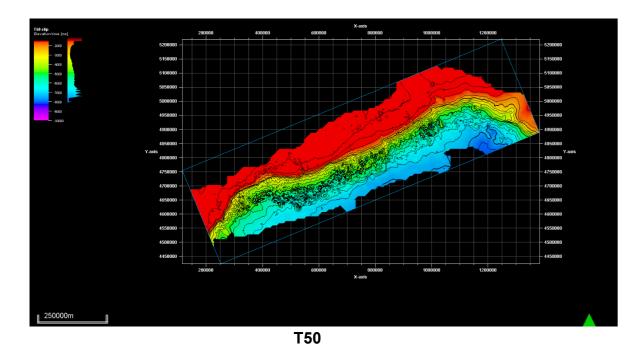
As a priority, the interval velocities at the wells were extracted from checkshot data when they are available (23 wells – Fig.3). As second source, the interval velocity is converted from the sonic log (6 wells – Fig.4).

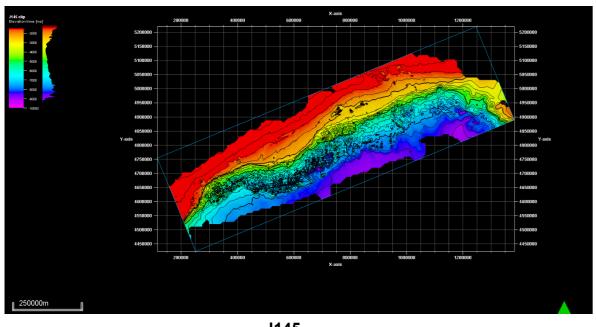
Well Time-to-Depth relationships (TZ) were based on these same items (checkshot and sonic) after calibration (see PL. 2.4).

The 11 last wells have no velocity data ("no TZ" tick). They were used as tertiary control to adjust the final pass of velocity co-kriging (see PL. 3.1).



Seafloor

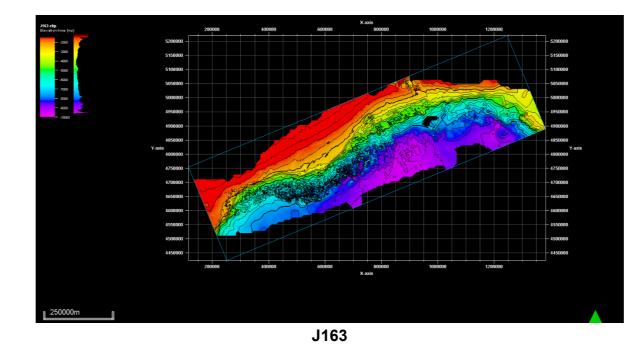


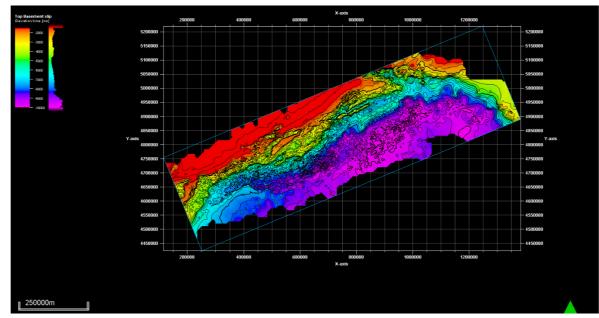


J145

## **Database Construction for Velocity Modeling**

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Top Basement

#### Main horizons

5 main gridded horizons were provided in TWT, and cover most of the AOI. They will be used to guide the velocity interpolation:

- Seafloor: totally gridded (200 x 200 m) in the AOI
- T50: gridded (200 x 200 m) without any gap
- J145: gridded (200 x 200 m) without any gap
- J163: gridded (200 x 200 m) with small gaps (1300 km<sup>2</sup>)
- Top Basement: gridded (200 x 200 m) without any gap

#### Salt

5 salt grids were provided in TWT (50 x 50m), representing 3 sets of salt structures (diapirs and canopies):

- to be joined at J163
- between T50 and J145
- area of Sable Island, mainly developed between J145 and J163

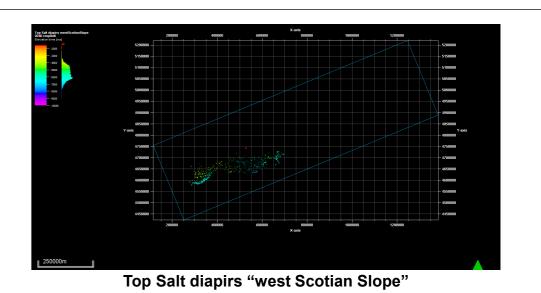
A global strategy of horizon editing is exposed in PL. 1.8.

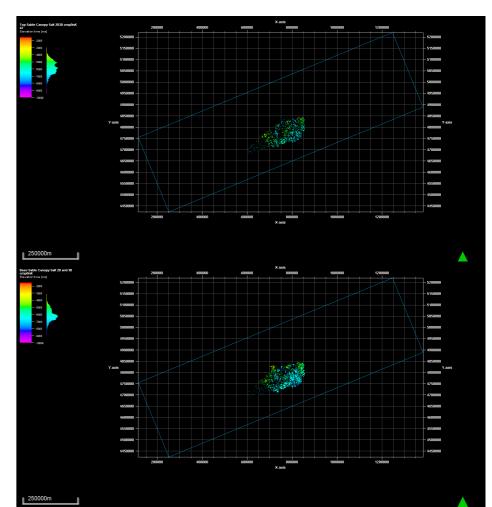
### **TWT** horizons

• "Top Salt diapirs west Scotian Slope": top salt representing the local western salt diapirs emerging from Late Jurassic layers along one third of the AOI length. Its base salt is supposed

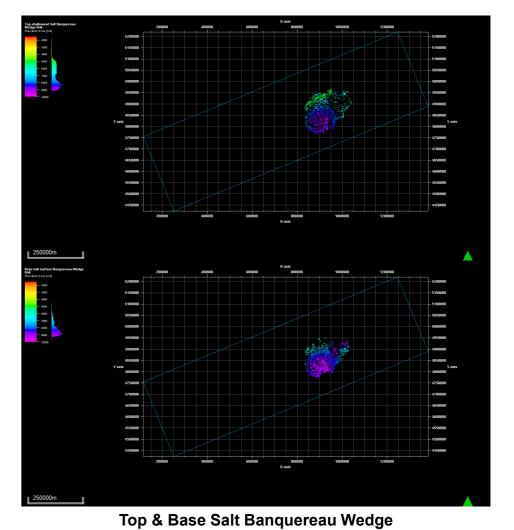
• "Top & Base Sable Canopy Salt": top and base of central salt canopy mainly developed

• "Top & Base Salt Banquereau Wedge": top and base of eastern diapir/canopy complex in the



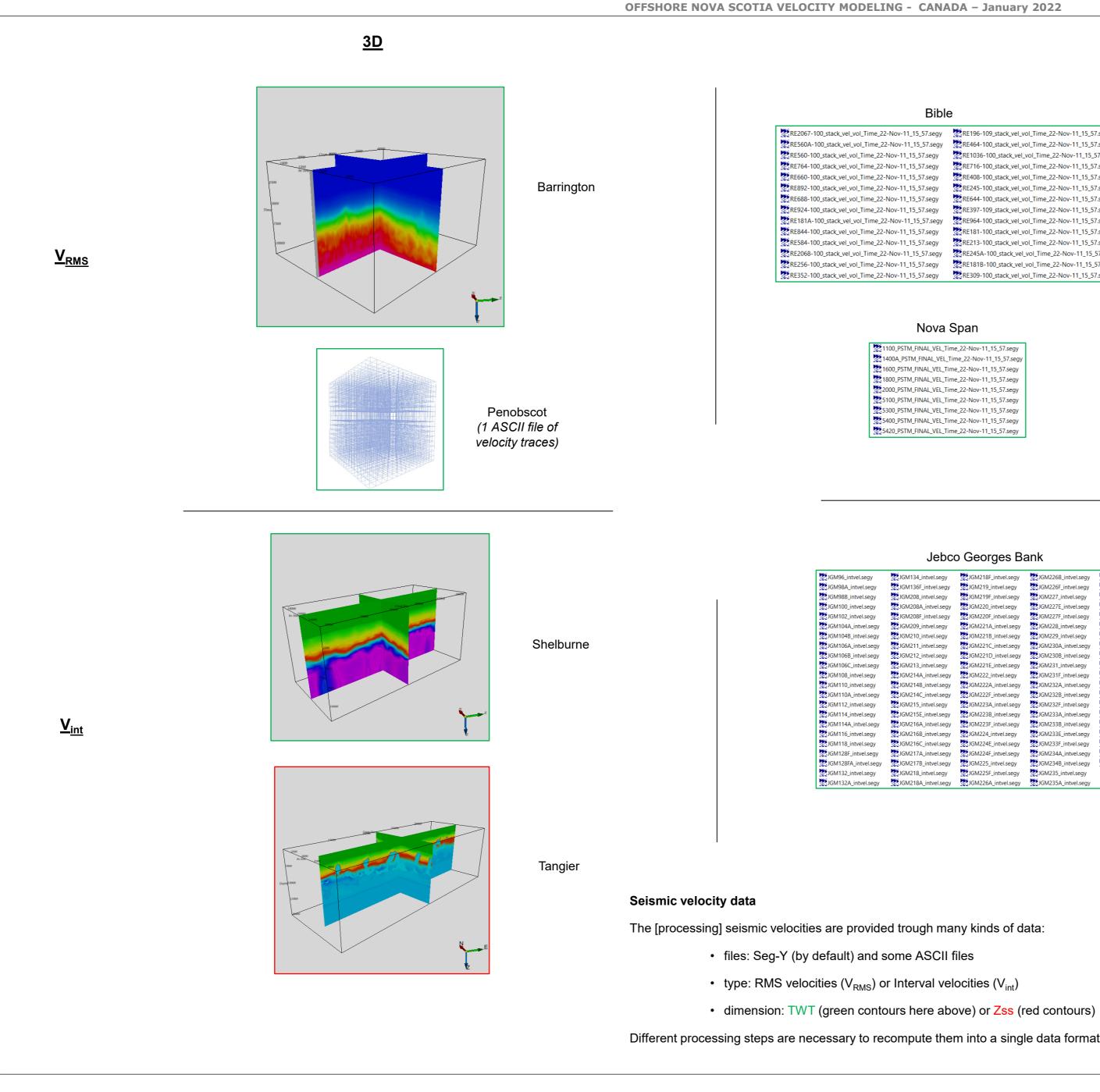


Top & Base Sable Canopy Salt



PL. 1.3

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<u>2D</u>

#### Bible

_15_57.segy	RE196-109_stack_vel_vol_Time_22-Nov-11_15_57.segy
1_15_57.segy	RE464-100_stack_vel_vol_Time_22-Nov-11_15_57.segy
15_57.segy	RE1036-100_stack_vel_vol_Time_22-Nov-11_15_57.segy
15_57.segy	RE716-100_stack_vel_vol_Time_22-Nov-11_15_57.segy
15_57.segy	RE408-100_stack_vel_vol_Time_22-Nov-11_15_57.segy
15_57.segy	RE245-100_stack_vel_vol_Time_22-Nov-11_15_57.segy
15_57.segy	RE644-100_stack_vel_vol_Time_22-Nov-11_15_57.segy
15_57.segy	RE397-109_stack_vel_vol_Time_22-Nov-11_15_57.segy
1_15_57.segy	RE964-100_stack_vel_vol_Time_22-Nov-11_15_57.segy
15_57.segy	RE181-100_stack_vel_vol_Time_22-Nov-11_15_57.segy
15_57.segy	RE213-100_stack_vel_vol_Time_22-Nov-11_15_57.segy
_15_57.segy	RE245A-100_stack_vel_vol_Time_22-Nov-11_15_57.segy
15_57.segy	RE181B-100_stack_vel_vol_Time_22-Nov-11_15_57.segy
15_57.segy	RE309-100_stack_vel_vol_Time_22-Nov-11_15_57.segy

### Nova Span

21400A\_PSTM\_FINAL\_VEL\_Time\_22-Nov-11\_15\_57.segy 21600\_PSTM\_FINAL\_VEL\_Time\_22-Nov-11\_15\_57.segy 21800\_PSTM\_FINAL\_VEL\_Time\_22-Nov-11\_15\_57.segy 2000\_PSTM\_FINAL\_VEL\_Time\_22-Nov-11\_15\_57.segy \$100\_PSTM\_FINAL\_VEL\_Time\_22-Nov-11\_15\_57.segy 5300\_PSTM\_FINAL\_VEL\_Time\_22-Nov-11\_15\_57.segy \$400\_PSTM\_FINAL\_VEL\_Time\_22-Nov-11\_15\_57.segy \$420\_PSTM\_FINAL\_VEL\_Time\_22-Nov-11\_15\_57.segy

1A_PSTM_vels_ASCII	8C_PSTM_vels_ASCII	30_PSTM_vels_ASCII
1B_PSTM_vels_ASCII	9_PSTM_vels_ASCII	31_PSTM_vels_ASCII
2A_PSTM_vels_ASCII	10A_PSTM_vels_ASCII	32_PSTM_vels_ASCII
2B_PSTM_vels_ASCII	11_PSTM_vels_ASCII	33_PSTM_vels_ASCII
2C_PSTM_vels_ASCII	12_PSTM_vels_ASCII	34_PSTM_vels_ASCII
3A_PSTM_vels_ASCII	13_PSTM_vels_ASCII	35_PSTM_vels_ASCII
3B_PSTM_vels_ASCII	14_PSTM_vels_ASCII	36_PSTM_vels_ASCII
3C_PSTM_vels_ASCII	15_PSTM_vels_ASCII	37_PSTM_vels_ASCII
4A_PSTM_vels_ASCII	16_PSTM_vels_ASCII	38_PSTM_vels_ASCII
4B_PSTM_vels_ASCII	17_PSTM_vels_ASCII	39_PSTM_vels_ASCII
4C_PSTM_vels_ASCII	18_PSTM_vels_ASCII	40_PSTM_vels_ASCII
5A_PSTM_vels_ASCII	19_PSTM_vels_ASCII	41_PSTM_vels_ASCII
5B_PSTM_vels_ASCII	20_PSTM_vels_ASCII	42_PSTM_vels_ASCII
5C_PSTM_vels_ASCII	21_PSTM_vels_ASCII	43_PSTM_vels_ASCII
6A_PSTM_vels_ASCII	22_PSTM_vels_ASCII	44_PSTM_vels_ASCII
6B_PSTM_vels_ASCII	23_PSTM_vels_ASCII	45_PSTM_vels_ASCII
6C_PSTM_vels_ASCII	24_PSTM_vels_ASCII	46_PSTM_vels_ASCII
7A_PSTM_vels_ASCII	25_PSTM_vels_ASCII	47_PSTM_vels_ASCII
7B_PSTM_vels_ASCII	26_PSTM_vels_ASCII	48_PSTM_vels_ASCII
7C_PSTM_vels_ASCII	27_PSTM_vels_ASCII	49_PSTM_vels_ASCII
8A_PSTM_vels_ASCII	28_PSTM_vels_ASCII	
BB_PSTM_vels_ASCII	29_PSTM_vels_ASCII	

Penobscot (64 ASCII files of velocity traces)

### Jebco Georges Bank

M134_intvel.segy	JGM218F_intvel.segy	JGM226B_intvel.segy	JGM235F_intvel.segy
M136F_intvel.segy	GM219_intvel.segy	CJGM226F_intvel.segy	GM236A_intvel.seg
M208_intvel.segy	GM219F_intvel.segy	CJGM227_intvel.segy	GM236B_intvel.seg
M208A_intvel.segy	GM220_intvel.segy	ZJGM227E_intvel.segy	GM237A_intvel.seg
M208F_intvel.segy	ZGM220F_intvel.segy	SIGM227F_intvel.segy	ZJGM237B_intvel.seg
M209_intvel.segy	CIGM221A_intvel.segy	🖉 JGM228_intvel.segy	Contemporary Content and Conte
M210_intvel.segy	CJGM221B_intvel.segy	🕅 JGM229_intvel.segy	JGM238B_intvel.seg
M211_intvel.segy	CJGM221C_intvel.segy	🕅 JGM230A_intvel.segy	CM239A_intvel.seg
M212_intvel.segy	CJGM221D_intvel.segy	CIGM230B_intvel.segy	Contemporary Content State Sta
M213_intvel.segy	CJGM221E_intvel.segy	CJGM231_intvel.segy	Contraction Contractico Contra
M214A_intvel.segy	GM222_intvel.segy	CJGM231F_intvel.segy	CJGM240_intvel.segy
M214B_intvel.segy	CJGM222A_intvel.segy	CJGM232A_intvel.segy	GM241A_intvel.seg
M214C_intvel.segy	GM222F_intvel.segy	JGM232B_intvel.segy	JGM241B_intvel.seg
M215_intvel.segy	JGM223A_intvel.segy	JGM232F_intvel.segy	JGM242_intvel.segy
M215E_intvel.segy	JGM223B_intvel.segy	JGM233A_intvel.segy	JGM243A_intvel.seg
M216A_intvel.segy	CIGM223F_intvel.segy	ZJGM233B_intvel.segy	JGM243B_intvel.seg
M216B_intvel.segy	CJGM224_intvel.segy	ZJGM233E_intvel.segy	SGM244A_intvel.seg
M216C_intvel.segy	Contemporary Conte	XJGM233F_intvel.segy	Contemporary Content State Sta
M217A_intvel.segy	CJGM224F_intvel.segy	CJGM234A_intvel.segy	CM245A_intvel.seg
M217B_intvel.segy	CJGM225_intvel.segy	CJGM234B_intvel.segy	Contraction Contractic Con
M218_intvel.segy	CJGM225F_intvel.segy	CJGM235_intvel.segy	
M218A_intvel.segy	JGM226A_intvel.segy	JGM235A_intvel.segy	

#### Jebco East

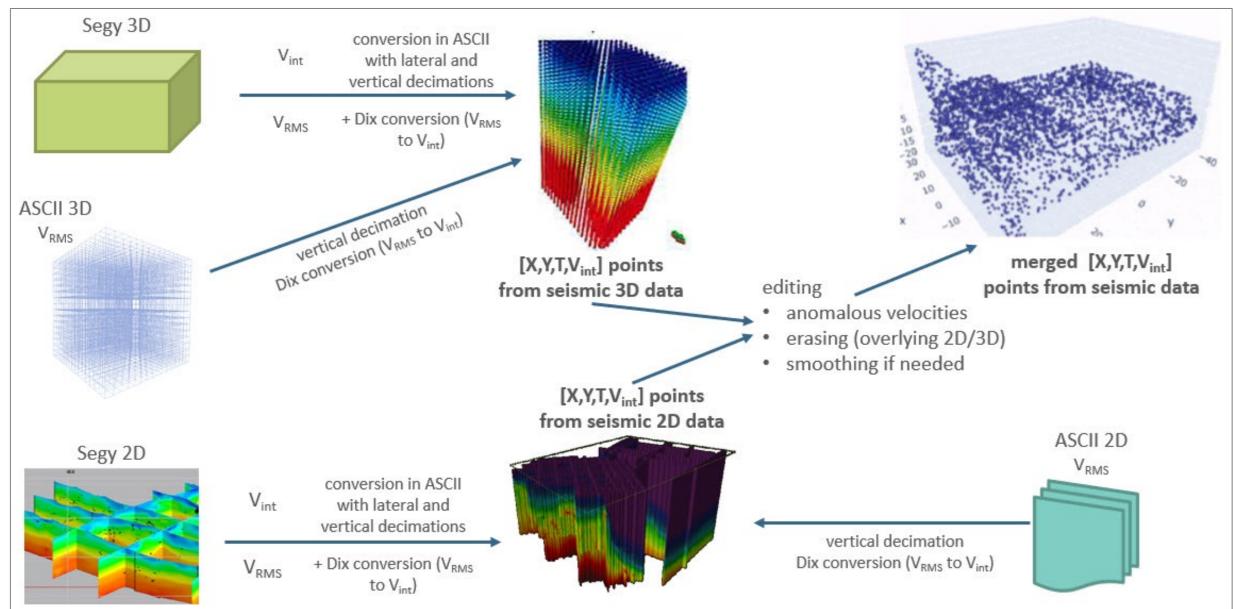
ZEBCO\_2013\_Depth\_Mig\_Velocity\_Interval\_J05\_05.SGY WJEBCO\_2013\_Depth\_Mig\_Velocity\_Interval\_J08\_08.SGY ZEBCO\_2013\_Depth\_Mig\_Velocity\_Interval\_J09\_09.SGY WJEBCO\_2013\_Depth\_Mig\_Velocity\_Interval\_J11\_11.SGY JEBCO\_2013\_Depth\_Mig\_Velocity\_Interval\_J13\_13.SGY

### Sable Island

Sable\_Island\_2013\_Depth\_Mig\_Velocity\_Interval\_L187.SGY Sable\_Island\_2013\_Depth\_Mig\_Velocity\_Interval\_L369.SGY Sable\_Island\_2013\_Depth\_Mig\_Velocity\_Interval\_L405.SGY Sable\_Island\_2013\_Depth\_Mig\_Velocity\_Interval\_L613.SGY

Different processing steps are necessary to recompute them into a single data format: 3D V<sub>int</sub> pointsets (i.e. [X,Y,T,V<sub>int</sub>] points)

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### Phase 2: 3D interpolation of seismic velocities through a stratigraphic model

A stratigraphic model is built using all the horizons (main ones and salt) after editing them (adjustment to remove the crossing zones, smoothing, recreation of separated diapir/canopy structures), deep enough to handle all the seismic data.

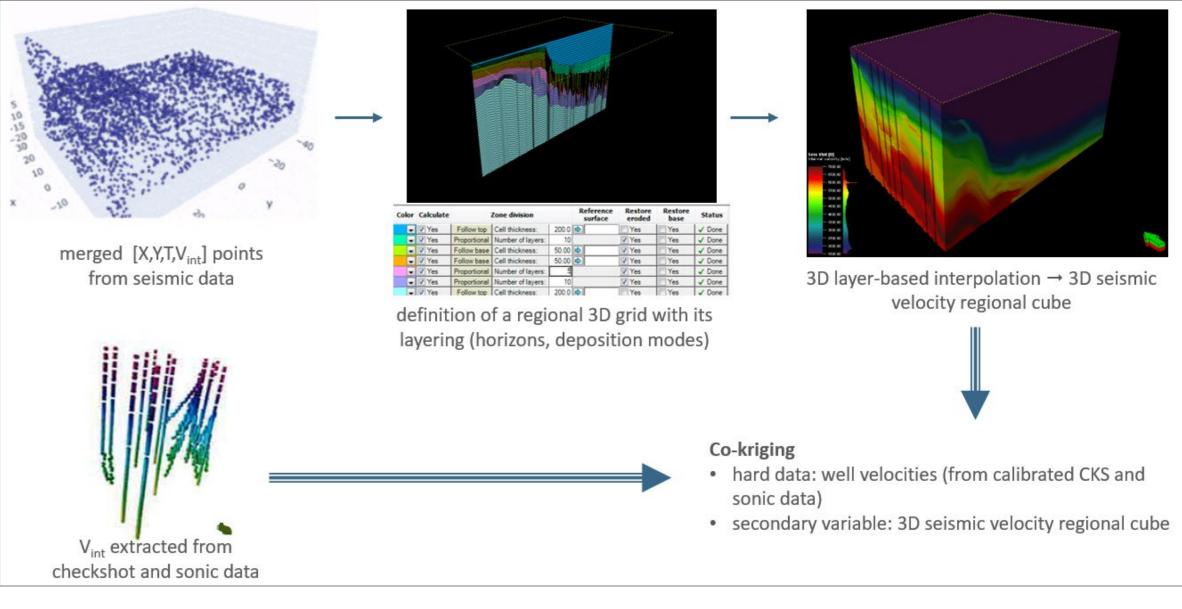
Different zones of layering are set between the edited horizons: regular layering in the sedimentary/reservoir zones, constant layer/velocity in the salt and water, broad layering in the basement unknown velocity zone.

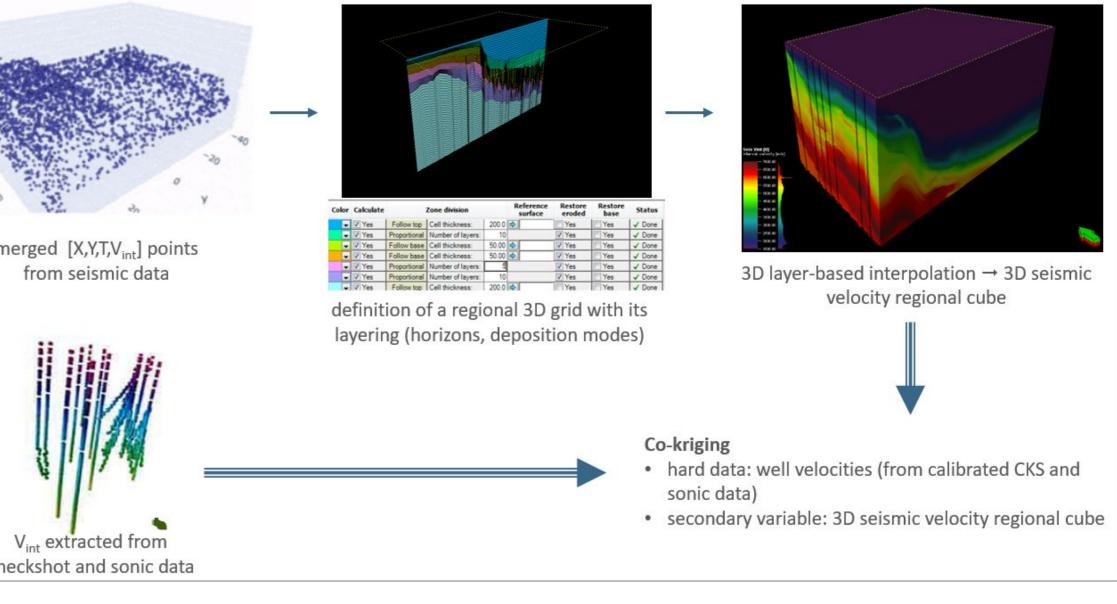
A global interpolation of the seismic velocities is then performed along the stratigraphy to get a complete 3D seismic velocity regional cube.

#### Phase 3: Co-kriging of the calibrated well velocities with the seismic velocity cube

Once calibrated to the horizons, markers and in accordance with the checkshot times, the well velocities can be co-kriged in the same stratigraphic model, using as secondary variable the 3D seismic velocity regional cube.

Such co-kriging preserves the calibrated TZ laws, consequently further residual correction would not be necessary (the residuals are corrected/estimated previously to the co-kriging).





### Workflow

### Phase 1: Creation of a merged set of [X,Y,T,V<sub>int</sub>] points from raw seismic velocities

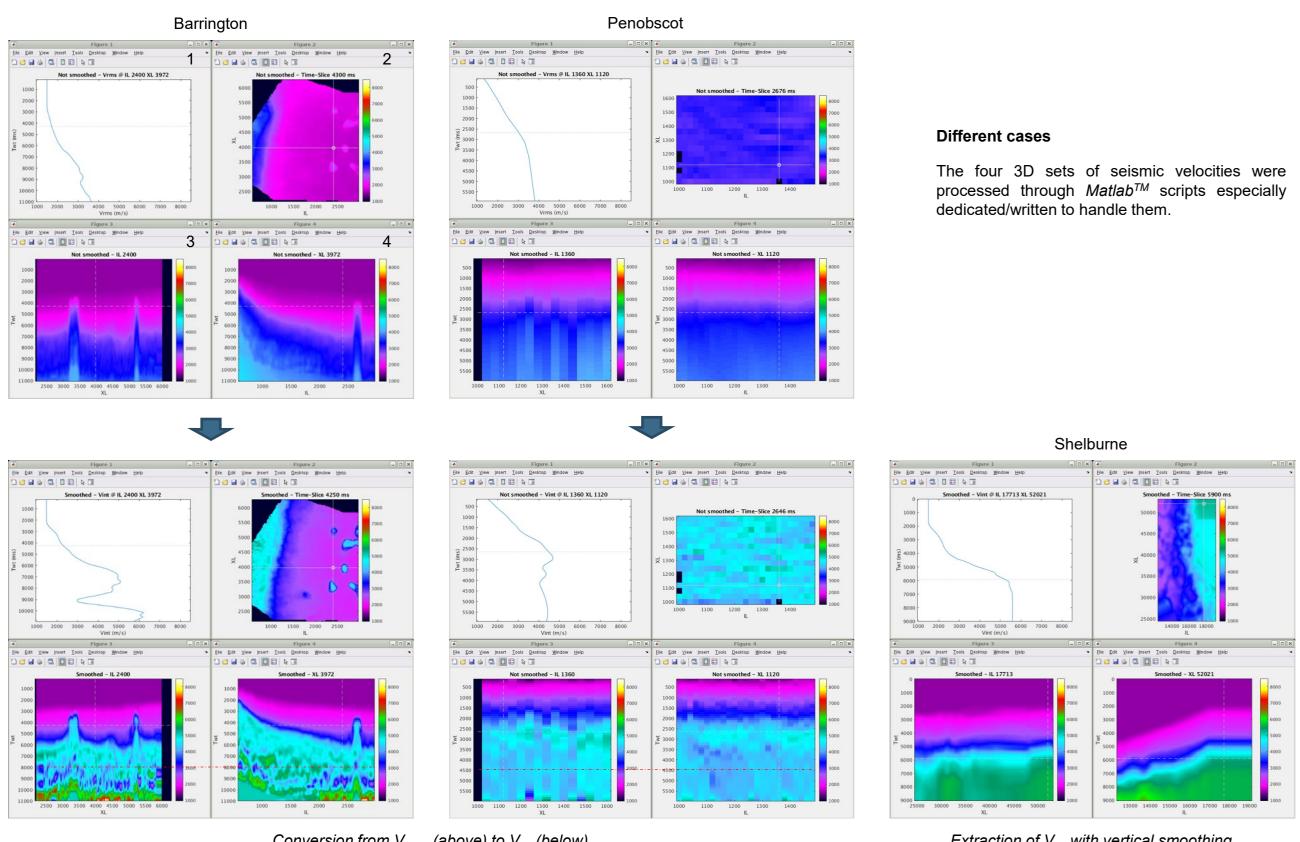
All the different sets of data were individually transformed into interval velocities via various programming scripts (run in *Matlab*<sup>TM</sup>):

- · via Dix conversions if quadratic velocities (RMS)
- directly taken as V<sub>int</sub> when they were available; when both quadratic and interval velocities were available, the former ones were favored (indeed the corresponding interval velocities presented either a blocky shape - see PL. 1.7 with Jebco Georges Bank example - or a "quantum effect", i.e. when Dix conversion was applied on the Segy format without upscaling these quadratic velocities that were oversampled, resulting a very limited range of interval velocities)

The editing of anomalous velocities was done in a first step before the merging: removing obviously wrong velocities, cropping, smoothing, upscaling them to regular 100-ms intervals (see PL. 1.6 and -.7). Actually, supplementary stages of editing were deemed necessary and applied before the final version of the seismic velocities interpolation (see PL. 2.5 to -.7)

Concerning the seismic velocities available in depth instead of TWT, scripts were also created to make them convert from Zss to TWT by their own values (once differentiated, a velocity may also be seen as TZ law).

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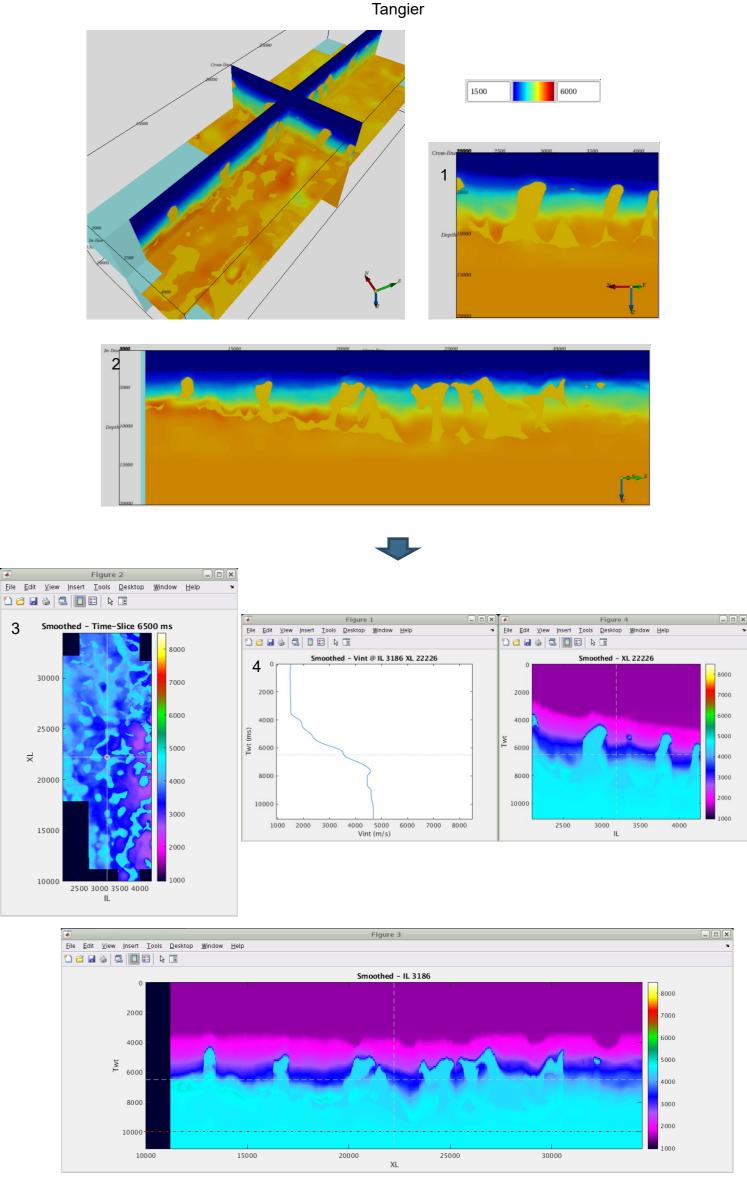
Conversion from  $V_{RMS}$  (above) to  $V_{int}$  (below) with vertical smoothing and time clipping (red line) (1- trace, 2- timeslice, 3- IL section, 4- XL section)

Extraction of V<sub>int</sub> with vertical smoothing and no time clipping

#### 3D workflow

The scripts enabled to visualize trough random sections the degree of the "original smoothing" after an upscaling to 100-ms samples and a lateral decimation of 200 m.

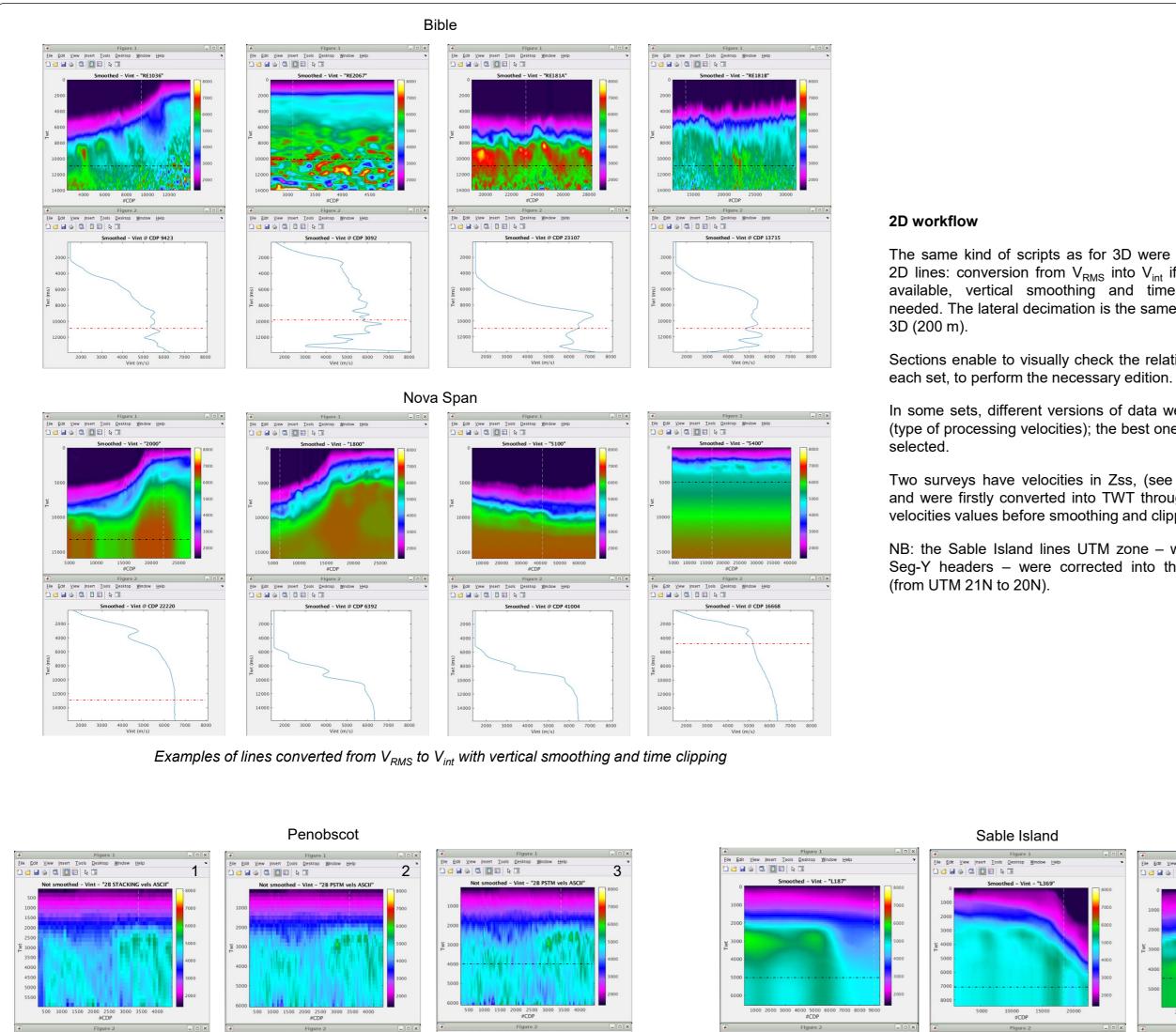
The irregular/odd variations of velocities in the deep layers, deemed as not natural, or totally constant ending parts (in Tangier) were clipped along a constant time line (displayed in red).



Conversion from Zss (above) to TWT (below) of original V<sub>int</sub> with slight vertical smoothing and time clipping (red line) (1- XL, 2- IL, 3- timeslice, 4- trace)

3

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ls <u>D</u>esktop <u>W</u>indow <u>H</u>elp

Not smoothed - Vint @ CDP 3400

2000 3000 4000 5000 6000 7000 8000 Vint (m/s)

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le Edit View Insert Tools Desktop Window Help

Not smoothed - Vint @ CDP 3400

4000 5000

6000

2000 3000

1000 -1500 -2000 -(32500 -33000 -4000 -4500 -5500 -

<u>File Edit View Insert Tools Desktop Window Help</u>

3000

Not smoothed - Vint @ CDP 3400

4000 5000 Vint (m/s)

Selection of one velocity version (PSTM – 2) instead of another (STACKING – 1)

Vertical smoothing and time clipping of the selected version (3)

6000

1 😂 🖬 🌢 🗔 🖪 🖽 🗎 🖬

4000 4500 -

5000

### **Preparing seismic velocity – 2D**

2000

Eile Edit ⊻iew Insert

2000 -3000 -

Twt (ms) 2000 -

6000 -7000

Tools Desktop Window Help

Smoothed - Vint @ CDP 8975

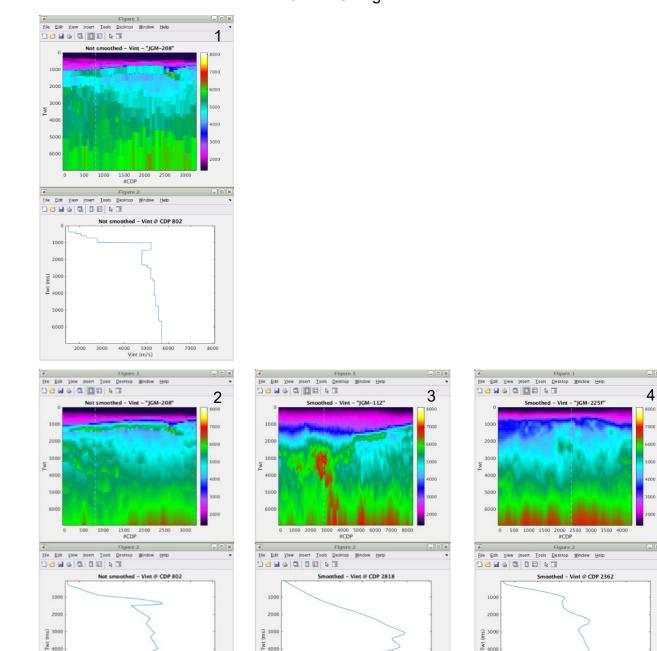
) 😂 🖬 🕹 🗐 🖬 🖬 🖬 🖬

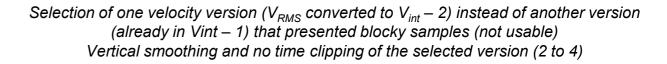
2000 3000

3000

The same kind of scripts as for 3D were used for the 2D lines: conversion from  $V_{\text{RMS}}$  into  $V_{\text{int}}$  if not already available, vertical smoothing and time clipping if needed. The lateral decimation is the same taken as for

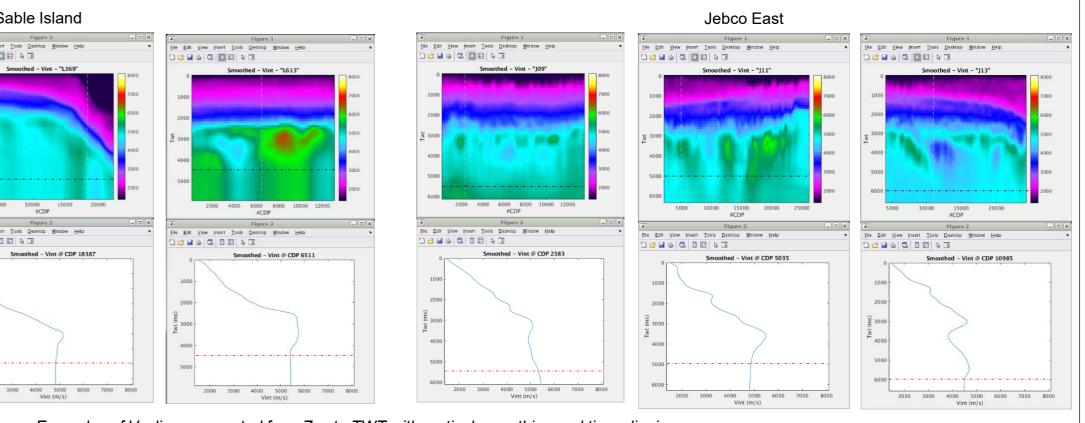
- Sections enable to visually check the relative quality of
- In some sets, different versions of data were available (type of processing velocities); the best one was always
- Two surveys have velocities in Zss, (see here below) and were firstly converted into TWT through their own velocities values before smoothing and clipping.
- NB: the Sable Island lines UTM zone written in the Seg-Y headers - were corrected into the good one





2000 3000 4000 5000 6000 7000 8000 Vint (m/s)

2000 3000 4000 5000 6000 7000 8000 Vint (m/s)



2000 3000 4000 5000 6000 7000 8000 Vint (m/s)

Examples of V<sub>int</sub> lines converted from Zss to TWT with vertical smoothing and time clipping

### PL. 1.7

### Jebco Georges Bank

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### Overall strategy of editing

- 1. Make consistent the 5 main horizons
- 2. Work on the salt the 3 salt packs (western diapirs, "Sable" central canopies, "Banquereau" eastern diapirs) to recreate, isolate and sort all the 10 horizons in a suitable order (with no internal crossing)

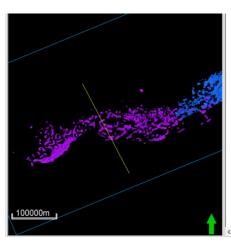
### **Objectives/ Preliminary constraints**

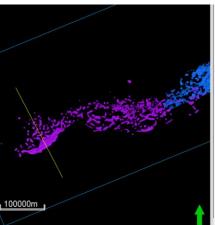
- Full-gridding for all the available horizons in the whole AOI
- No crossing between any horizon → create a sequential layering by adjusting them in space (filling via gridding) and vertically (cropping if crossing: J145 lowered to T50, then J163 lowered to J145, then Top Basement lowered to J163)

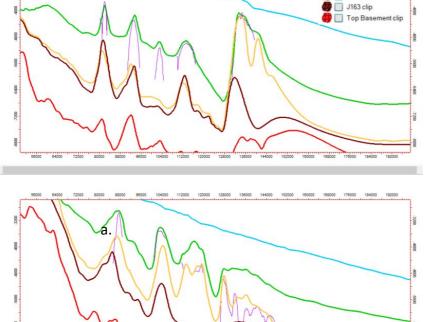
T50 clip

J145 clip

• Simulating the salt diapirs piercing the overlying horizons  $\rightarrow$  horizons wrapping the diapirs







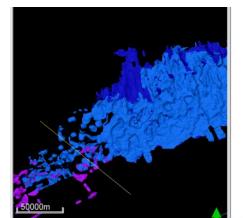
Top Salt diapirs westScotianSlop

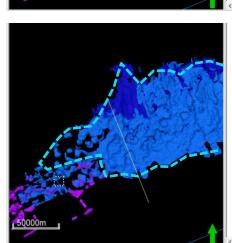
### **General rules**

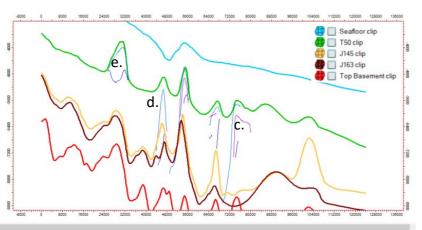
- 1. Slight smoothing the salt horizons
- 2. Top salt clipped with T50
- 3. Its edges merged with J163 (verticalization of the flanks)

### Specific rules for western diapirs

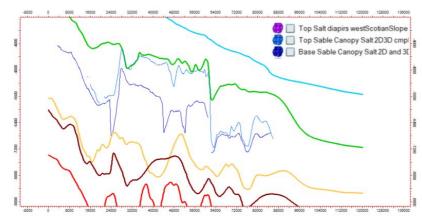
- a. J145 will be pierced by top diapir (i.e. top J145 set at top diapir)
- b. Top diapir stopped at J163







112000 120000 128000 138000 144000 152000 180000 188000 178000

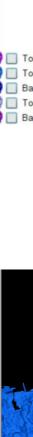


### Specific rules for diapir area

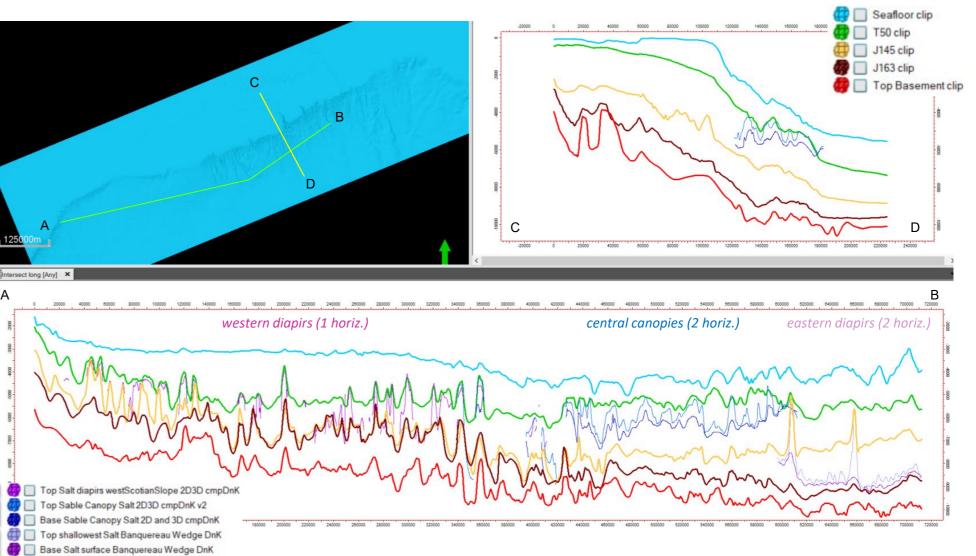
- c. When both exist, top diapir pierced by top canopy (i.e. top diapir extended shallower);
- d. Within diapir area, top canopy set as top diapir (merged to it, same rules)
- e. In the canopy area, see below

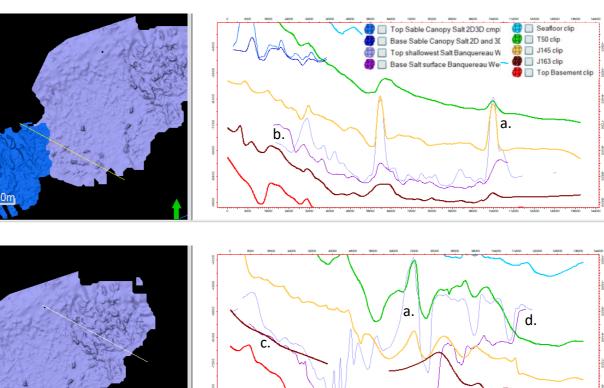
### Specific rules for canopy

- Define a boundary where the 1. isolated canopy will exist → extend top and base canopy to it (gridding)
- 2. Consider the canopy as in internal layer between T50 and J163  $\rightarrow$  thickness set to 0+ out of the boundary









### Specific rules for eastern diapirs

Same as for central Canopy (common limits for top and base; considered as new internal layer between J145 and J163):

- a. J145 will be pierced by top Banquereau salt diapir (i.e. top J145 set at top diapir)
- b. Base clipped by the Top
- c. Top and Base salt stopped at J163
- d. Top and Base clipped by T50

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#### Central canopy

- The Sable canopy system can be divided into three subgroups (Figure 3):
- located in the [T50; J145] interval
- B. Lower Canopy: the extension of Upper Canopy in the [J145; J163] interval
- Shelburne diapirs

Time thickness maps of top/base canopy vs. J145 enable to draw the polygons that will cut the continuous canopy into its 2 Upper and Lower continuous levels (Figure 4):

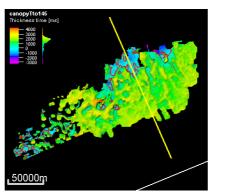




Figure 4: Time thickness maps of [Top Canopy; J145] and [Base Canopy; J145]

In the central continuous part, small parts of the canopy are located below J145 (see blue zones delimiting by red contours in Figure 5): they are negligible and will be clipped.

In the western part of the Sable canopy complex, the isolated salt parts are mostly present above J163. The very deep parts of the canopy that are defined below J163 will be clipped (Figure 6); and as J145 is very close to J163 in this area (see same Figure), the isolated parts will be thus clipped to be preserved above the yellow J145 horizon.

NB: in the westernmost part of Sable salt horizons, the remaining parts of top Canopy will be merged with Shelburne diapirs (see PL. 1.10).

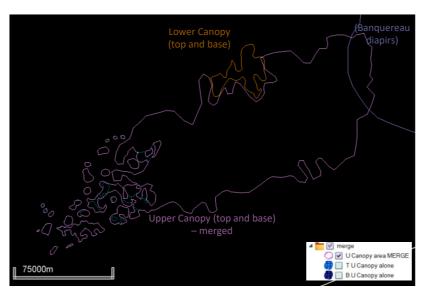


Figure 7: Sable canopy system defined by 3 subgroups

### Whole AOI

The 5 main horizons were gridded and adjusted as previously mentioned (cropping strategy: "the shallower, the more confident", i.e. the 5 horizons are cropped from base to top of the 3D grid). To insert the next salt horizons without any crossing, a space of 5 ms was left between each main horizon (see Figure 1).

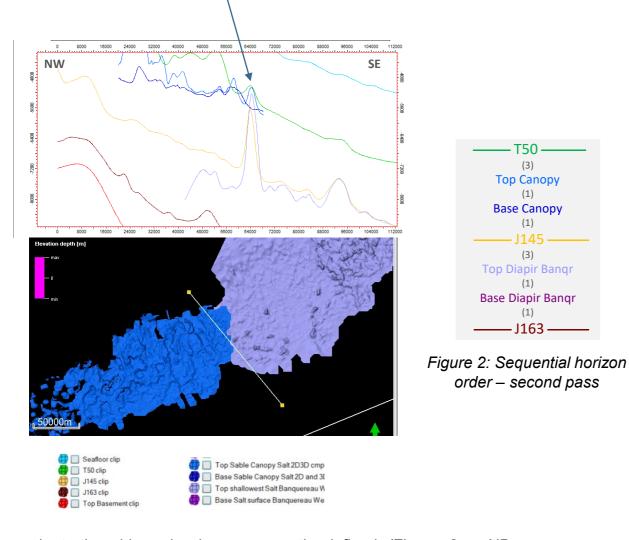


Figure 1: Sequential horizon order – first pass

#### Banquereau (eastern area)

After gridding and adjusting the 5 main horizons, two editing phases were run in Banquereau diapir area:

- J145 was set above top and base Banguereau diapir (J145 wrapping the top)
- Base Sable canopy was set above top Banquereau diapir (NB: there is no intersection between top Sable canopy and Banquereau salt horizons)



A second stratigraphic order is consequently defined (Figure 2 - NB: between parenthesis = minimal space in ms TWT between subsequent horizons to prevent any crossing)

A. Upper Canopy: a continuous canopy zone defined by top and base salt horizon and

C. Isolated parts of Upper Canopy, equivalent of diapir structures as defined by the eastern

ΝΝΜ

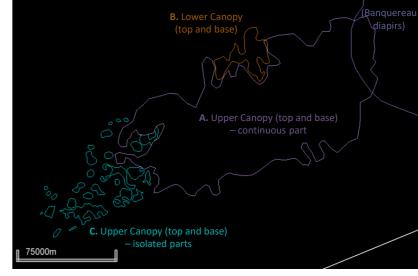


Figure 3: Sable canopy system defined by 3 subgroups

140000

 Upper Canopy (top and base) - continuous part

B. Lower Canopy (top and base)

160000

180000

Seafloor clip

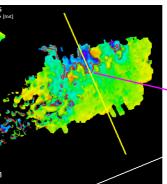
T50 clip J145 clip J163 clip Top Basement

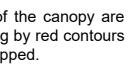
Top Sable Canopy Salt 2D3D cmp

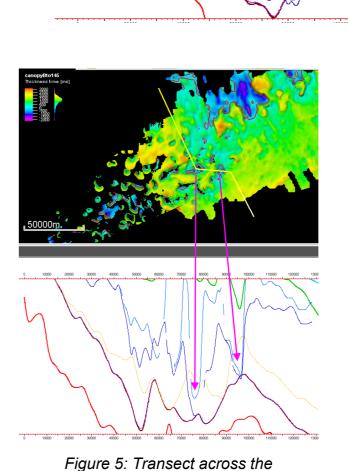
Base Sable Canopy Salt 2D and 30

200000

SSE







continuous part

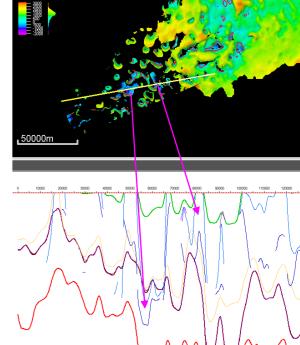
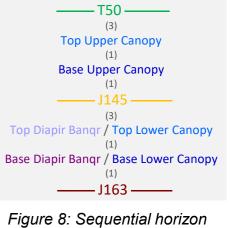


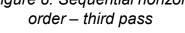
Figure 6: Transect across the isolated parts

Top Salt diapirs westScotianSlope Top Sable Canopy Salt 2D3D cmp Base Sable Canopy Salt 2D and 30

A second pass of editing enables to merge some near isolated parts to the main continuous canopy (cf. Figure 7 with Figure 6). These merging polygons were extended/checked in accordance with the western Shelburne diapirs that were joined to the canopy in these common areas.

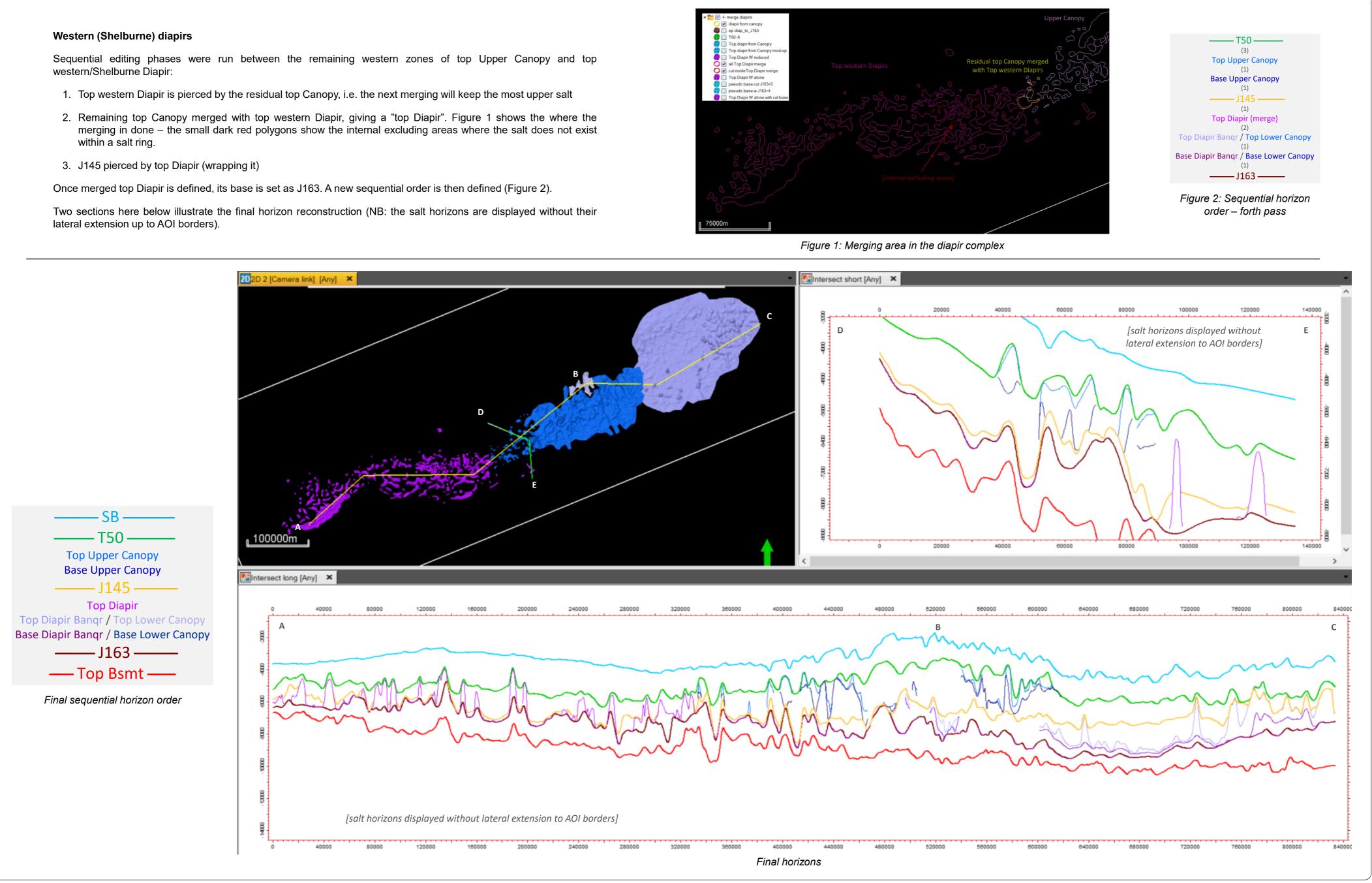
Lastly, to simplify the number of horizons, the Lower Canopy top and base were merged with Banquereau salt horizon (both sets located in the same interval and never overlaid by each other). It generates the sequential order as displayed in Figure 8.



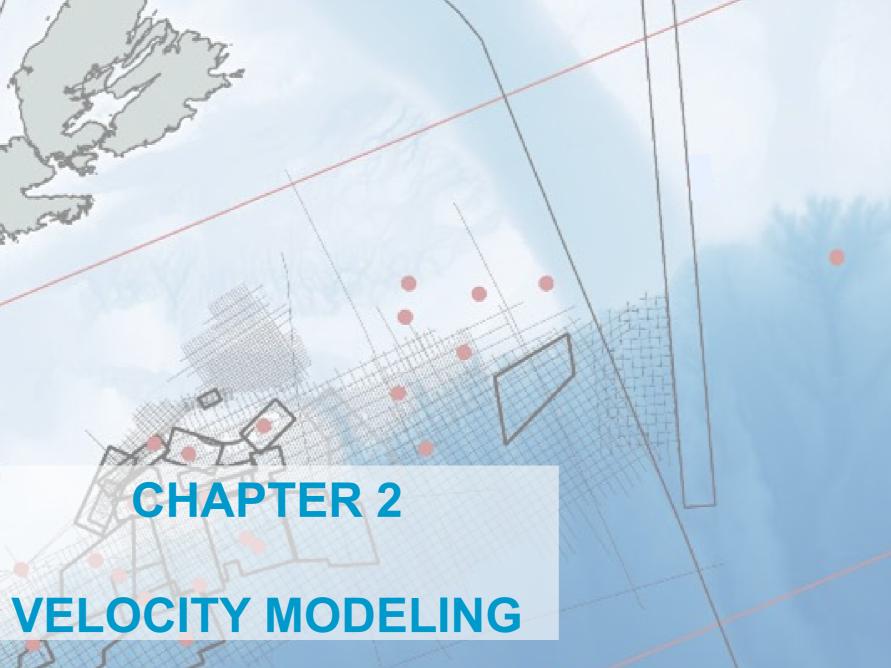


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- within a salt ring.



### Preparing horizons – Editing (2)



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Jack Stranderstand

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and

Stratty Martin 1

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### Making the skeleton

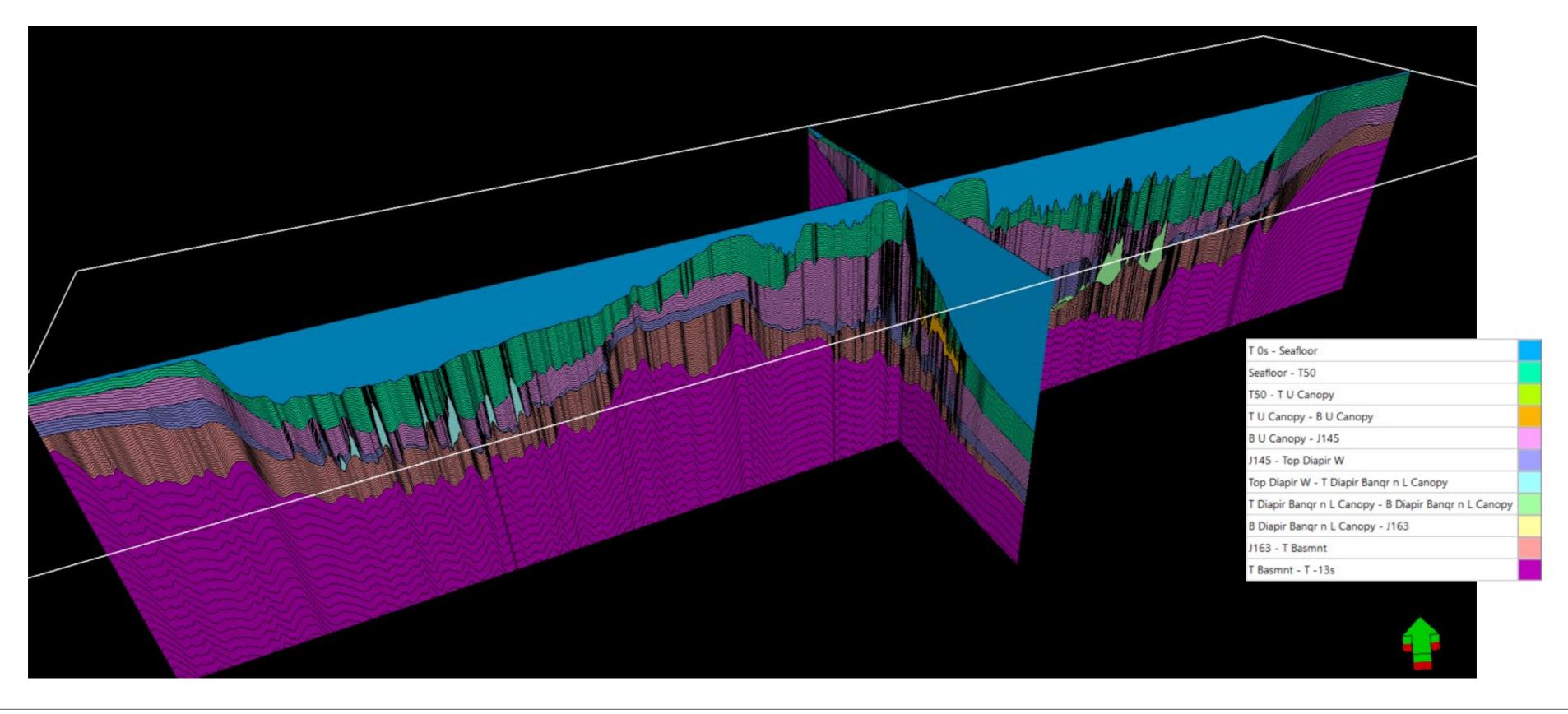
A blank 3D TWT grid was created using a *Simple Grid* process:

- Top defined at 0 ms TWT (MSL), base defined at 13 s
- Lateral limits set at AOI (same corner points and rotation): 358 km x 1224 km (438,000 km<sup>2</sup>)
- Lateral mesh set at 1 km (good compromise between smoothing and stratigraphic precision) – see Figure 1
- Zoning done with 10 horizons as defined in Figure 2: 11 zones are created from MSL to 13 s
- Layering done every 50 ms (Figure 3), except for:
  - water and salt zone: 1 layer with constant velocity (resp. 1500 and 4300 m/s)
  - in [Top Basement; +13 s] zone: 500-ms intervals

🖳 🖲 Sk	eleton only	
🥥 🔿 Ins	ert surfaces	
Top limit	Constant	~
		Z-value
	0	2 1000
Base limit	Constant	~
	-13000	Z-value

Automatic (from	n input data/boundary)	-		
User defined:	Get all settings from	n selected	Get limits	from selected
X min: 114000	<b></b>			
Y min: 4754000	*			
K max: 473000	Width:	359000	*	Expand
f max 5978000	Height	1224000	-	Shrink
Rotation:	\$ 292.38422065			

Figure 1: Lateral settings of the modeling grid



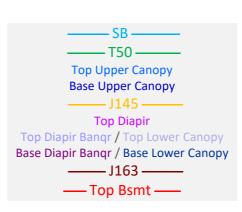


Figure 2: The 10 horizons

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mmon settings											
Build along: Along the pillars			2	Horizons with ste	on	elones					
Stand along. Vising the pindlo						l/fractions, start from:	To				
				melade proporeo	IId	gracuons, starrioni.	10	þ 🗼			
ne specific settings		12			-						
Zone division: Reference su	urface:		Restor	re eroded: [		Restore base:	?				
Name	Col	lor	Calculate	:	Zo	ne division		Reference surface	Restore	Restore	Status
T Os - Seafloor		*	✓ Yes	Proportional	•	Number of layers:	1		No	No	New
Seafloor - T50		*	✓ Yes	Follow base	•	Cell thickness:	50.00	\$	No	No	O New
T50 - T U Canopy		-	✓ Yes	Follow base	•	Cell thickness:	50.00	\$	No	No	O New
T U Canopy - B U Canopy		*	✓ Yes	Proportional	•	Number of layers:	1		No	No	O New
B U Canopy - J145		*	✓ Yes	Follow base	•	Cell thickness:	50.00	\$	No	No	New
J145 - Top Diapir W		*	✓ Yes	Follow base	•	Cell thickness:	50.00	\$	No	No	O New
Top Diapir W - T Diapir Bangr n L Canopy		*	✓ Yes	Proportional	•	Number of layers:	1		No	No	O New
T Diapir Bangr n L Canopy - B Diapir Bang	r i	•	✓ Yes	Proportional	•	Number of layers:	1		No	No	New
T Diapir bandr n L Canopy - b Diapir band		-	✓ Yes	Follow base		Cell thickness:	50.00	\$	No	No	New
B Diapir Bangr n L Canopy - J163			100 100								
		*	✓ Yes	Follow base	•	Cell thickness:	50.00	\$	No	No	New

Figure 3: Zoning and layering

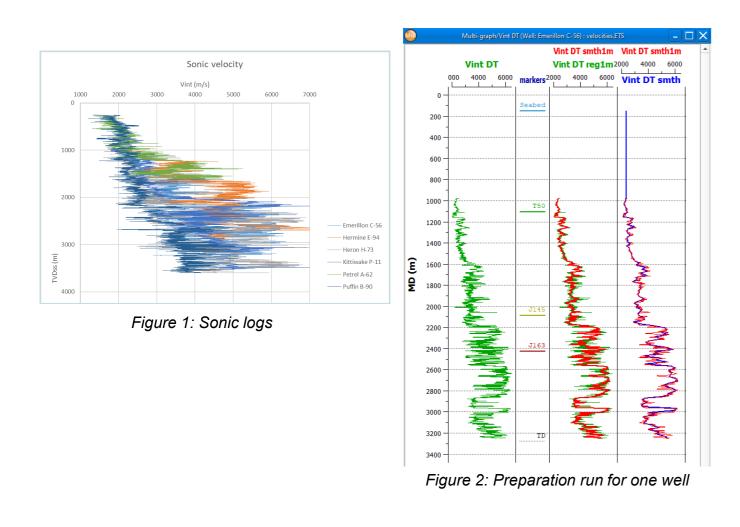
### **OFFSHORE NOVA SCOTIA VELOCITY MODELING - CANADA – January 2022**

### Wells with only sonic logs

To convert the well data (trajectory, markers, logs) from depth to time (TZ) for the 6 wells with only sonic log available as velocity data (Figure 1), different phases were applied.

A preparation workflow was first run in *EasyTrace*<sup>TM</sup>:

- V<sub>int</sub> computation in m MD from DT (green curve in Figure 2) with small editions if needed
- 1m-regularization
- Smoothing (red curve)
- 20m-regularization (blue curve) up to Seafloor



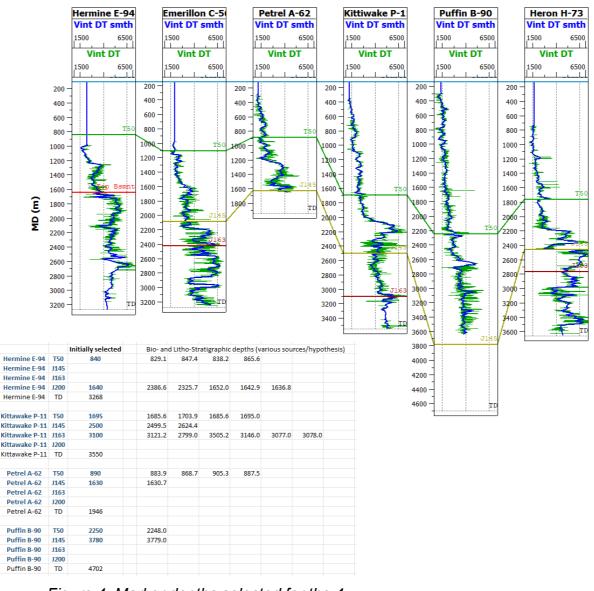
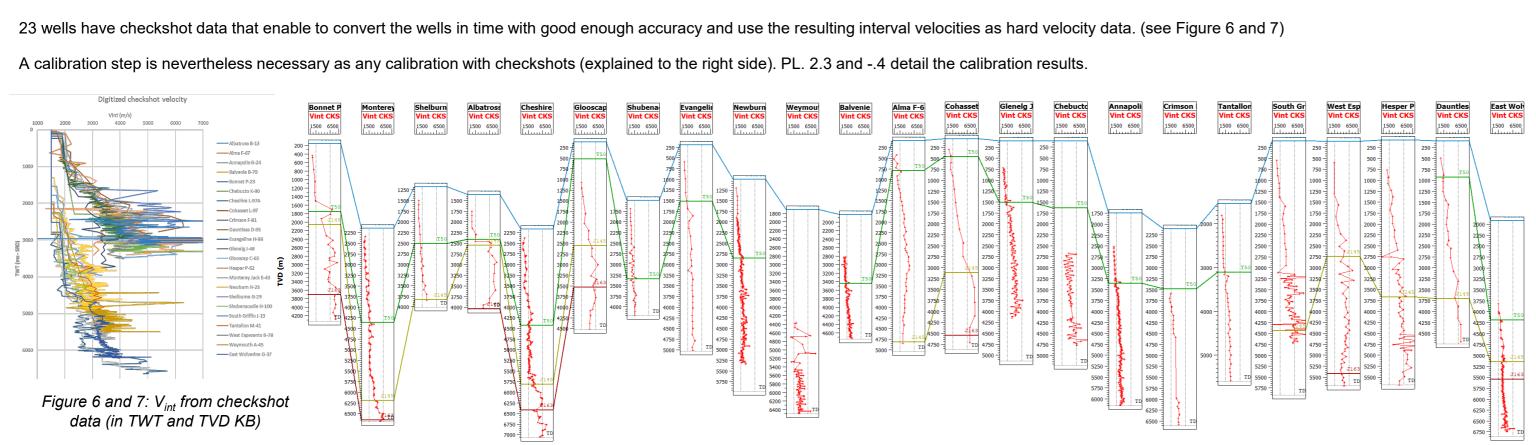


Figure 4: Marker depths selected for the 4 wells without geological markers

### Wells with checksot data



### Figure 3 displays the reprocessed sonic logs that can be used for the next phase: their calibration to the horizons to estimate the shallowest velocities not available in the sonic log (see methodology on the right side).

Besides, 4 wells out of the 6 ones do not have geological markers but only bio- and litho-stratigraphic information at different depths defined during various versions/vintages of interpretation. An attempt of setting the main horizons depths was done for those wells (see Figure 4).

Figure 3: Sonic logs prepared for the 6 wells

### Well – Time to Depth relationships (TZ) – Methodologies

The calibration is done along a "test 'n try" process:

- A velocity at the Seafloor is estimated for a first trial (V0) extrapolated/evaluated from the first defined log point (V1). It defines a static time shift of zero ms
- The velocity is linearly interpolated between the Seabed and the first V1 sonic point (italic red values in Figure 5)
- TWT values are thus computed all along the well path
- When the intersection of the well path with the main horizons will suggest a static shift value for the TZ law (an average or chosen value), the V0 value will be modified so that shift(V0) be equal to that value
- The calibration will provide final TZ relationships and calibrated V<sub>int</sub> logs
- The calibration is done along a "test 'n try" process:

#### PL. 2.3 and -.4 detail the calibration results.

Emerillon C-56	SB (m ss)	120	KB (m)	30	2150	shft(V0)	Hermine E-94	SB (m ss)	83	KB (m)	26	2200	shft(V0)	Heron H-73	SB (m ss)	105	KB (m	) 26	2000	shft(V0)	<b>Kittiv</b>
dev.	m TVDss	TWT	m TVD KB		Vint	0.0	11.	m TVDss	TWT	m TVD KB		Vint	0.0		m TVDss	TWT		B m MD KB	Vint	0.0	
Emerillon C-56	0	0	30	30.2	1500		Hermine E-94	0	0	26	26.0	1500		Heron H-73	0	0	26	26.0	1500		<b>Kittiw</b>
Emerillon C-56	118.8	158.4	149	149.0	1500		Hermine E-94	81.6	108.8	108	107.6	1500		Heron H-73	104.5	139.3	130	130.5	1500		<b>Kitti</b> w
Emerillon C-56	120	160	150	150	2150	V0	Hermine E-94	83	110	109	109	2200	V0	Heron H-73	105	141	131	131	2000	V0	<b>Kitti</b> w
Emerillon C-56	139.8	178.3	170	170.0	2155.6		Hermine E-94	103.0	128.6	129	129.0	2209.8		Heron H-73	125.0	160.1	151	151.0	2004.7		<b>Kitti</b> w
Emerillon C-56	159.8	196.9	190	190.0	2161.2		Hermine E-94	123.0	146.7	149	149.0	2219.5		Heron H-73	145.0	180.1	171	171.0	2009.4		<b>Kittin</b>
Emerillon C-56	179.8	215.3	210	210.0	2166.9		Hermine E-94	143.0	164.7	169	169.0	2229.1		Heron H-73	165.0	199.9	191	191.0	2014.2		<b>Kittin</b>
Emerillon C-56	199.8	233.8	230	230.0	2172.5		Hermine E-94	163.0	182.6	189	189.0	2238.7		Heron H-73	185.0	219.8	211	211.0	2019.0		<b>Kittin</b>
Emerillon C-56	219.8	252.2	250	250.0	2178.1		Hermine E-94	183.0	200.4	209	209.0	2248.4		Heron H-73	205.0	239.6	231	231.0	2023.7		<b>Kittin</b>
Emerillon C-56	239.8	270.5	270	270.0	2183.7		Hermine E-94	203.0	218.2	229	229.0	2258.0		Heron H-73	225.0	259.3	251	251.0	2028.5		Kittin
Emerillon C-56	259.8	288.8	290	290.0	2189.3		Hermine E-94	223.0	235.8	249	249.0	2267.6		Heron H-73	245.0	279.0	271	271.0	2033.3		Kittin
Emerillon C-56	279.8	307.1	310	310.0	2194.9		Hermine E-94	243.0	253.4	269	269.0	2277.3		Heron H-73	265.0	298.7	291	291.0	2038.0		Kittin
Emerillon C-56	299.8	325.3	330	330.0	2200.5		Hermine E-94	263.0	271.0	289	289.0	2286.9		Heron H-73	285.0	318.3	311	311.0	2042.8		Kittin
Emerillon C-56	319.8	343.4	350	350.0	2206.1		Hermine E-94	283.0	288.4	309	309.0	2296.5		Heron H-73	305.0	337.8	331	331.0	2047.6		Kittiw
Emerillon C-56	339.8	361.5	370	370.0	2211.8		Hermine E-94	303.0	305.8	329	329.0	2306.2		Heron H-73	325.0	357.3	351	351.0	2052.4		Kittiw
Emerillon C-56	359.8	379.6	390	390.0	2217.4		Hermine E-94	323.0	323.1	349	349.0	2300.2		Heron H-73	345.0	376.8	371	371.0	2052.4		Kittiw
Emerillon C-56	379.8	397.6	410	410.0	2223.0		Hermine E-94	343.0	340.4	369	369.0	2315.0		Heron H-73	365.0	396.2	391	391.0	2001.1		Kittiw
Emerillon C-56	399.8	415.6	430	410.0	2223.0		Hermine E-94	363.0	357.5	389	389.0	2325.4		Heron H-73	385.0	415.6	411	411.0	2007.9		Kittiw
Emerillon C-56 Emerillon C-56	419.8	415.6	450	450.0	2226.0		111.	363.0	357.5	409	409.0	2335.1		////	405.0	415.6	411		2000.7		1111
	419.0		450				Hermine E-94							Heron H-73				431.0			Kittiv
Emerillon C-56		451.4		470.0	2239.8		Hermine E-94	403.0	391.6	429	429.0	2354.3		Heron H-73	425.0	454.2	451	451.0	2076.2		Kittiw
Emerillon C-56	459.8	469.2	490	490.0	2245.4		Hermine E-94	423.0	408.6	449	449.0	2364.0		Heron H-73	445.0	473.5	471	471.0	2081.0		Kittiw
Emerillon C-56	479.8	487.0	510	510.0	2251.1		Hermine E-94	443.0	425.5	469	469.0	2373.6		Heron H-73	465.0	492.7	491	491.0	2085.7		Kittiw
Emerillon C-56	499.8	504.7	530	530.0	2256.7		Hermine E-94	463.0	442.3	489	489.0	2383.2		Heron H-73	485.0	511.8	511	511.0	2090.5		Kittiw
Emerillon C-56	519.8	522.5	550	550.0	2262.3		Hermine E-94	483.0	459.1	509	509.0	2392.9		Heron H-73	505.0	530.9	531	531.0	2095.3		Kittiw Kittiw
Emerillon C-56	539.8	540.1	570	570.0	2267.9		Hermine E-94	503.0	475.7	529	529.0	2402.5		Heron H-73	525.0	550.0	551	551.0	2100.0		Kittiw
Emerillon C-56	559.8	557.7	590	590.0	2273.5		Hermine E-94	523.0	492.4	549	549.0	2412.1		Heron H-73	545.0	569.0	571	571.0	2104.8		Kittiw
Emerillon C-56	579.8	575.3	610	610.0	2279.1		Hermine E-94	543.0	508.9	569	569.0	2421.8		Heron H-73	565.0	588.0	591	591.0	2109.6		Kittiw
Emerillon C-56	599.8	592.8	630	630.0	2284.7		Hermine E-94	563.0	525.4	589	589.0	2431.4		Heron H-73	585.0	606.9	611	611.0	2114.4		Kittiw
Emerillon C-56	619.8	610.3	650	650.0	2290.4		Hermine E-94	583.0	541.8	609	609.0	2441.1		Heron H-73	605.0	625.8	631	631.0	2119.1		Kittiw
Emerillon C-56	639.8	627.8	670	670.0	2296.0		Hermine E-94	603.0	558.2	629	629.0	2450.7		Heron H-73	625.0	644.7	651	651.0	2123.9		Kittiw
Emerillon C-56	659.8	645.2	690	690.0	2301.6		Hermine E-94	623.0	574.4	649	649.0	2460.3		Heron H-73	645.0	663.5	671	671.0	2128.7		Kittiw
Emerillon C-56	679.8	662.5	710	710.0	2307.2		Hermine E-94	643.0	590.7	669	669.0	2470.0		Heron H-73	665.0	682.3	691	691.0	2133.4		Kittiv Kittiv
Emerillon C-56	699.8	679.8	730	730.0	2312.8		Hermine E-94	663.0	606.8	689	689.0	2479.6		Heron H-73	685.0	701.0	711	711.0	2138.2		Kittiv Kittiv
Emerillon C-56	719.8	697.1	750	750.0	2318.4		Hermine E-94	683.0	622.9	709	709.0	2489.2		Heron H-73	705.0	719.7	731	731.0	2143.0	V1	Kittiw
Emerillon C-56	739.8	714.3	770	770.0	2324.0		Hermine E-94	703.0	639.0	729	729.0	2498.9		Heron H-73	725.0	738.9	751	751.0	2023.1		Kittiw
Emerillon C-56	759.8	731.5	790	790.0	2329.7		Hermine E-94	723.0	655.0	749	749.0	2508.5		Heron H-73	745.0	758.4	771	771.0	2077.7		Kittiw
Emerillon C-56	779.8	748.7	810	810.0	2335.3		Hermine E-94	743.0	670.9	769	769.0	2518.1		Heron H-73	765.0	778.0	791	791.0	1999.9		<b>Kittin</b>
Emerillon C-56	799.8	765.8	830	830.0	2340.9		Hermine E-94	763.0	686.7	789	789.0	2527.8		Heron H-73	785.0	797.6	811	811.0	2086.0		Kittin
Emerillon C-56	819.8	782.9	850	850.0	2346.5		Hermine E-94	783.0	702.5	809	809.0	2537.4		Heron H-73	805.0	816.9	831	831.0	2066.9		Kittiw
Emerillon C-56	839.8	799.9	870	870.0	2352.1		Hermine E-94	803.0	718.3	829	829.0	2547.0		Heron H-73	825.0	836.3	851	851.0	2057.9		<b>Kitti</b> w
Emerillon C-56	859.8	816.9	890	890.0	2357.7		Hermine E-94	823.0	733.9	849	849.0	2556.7		Heron H-73	845.0	855.9	871	871.0	2025.6		<b>Kitti</b> w
Emerillon C-56	879.8	833.8	910	910.0	2363.3		Hermine E-94	843.0	749.5	869	869.0	2566.3		Heron H-73	865.0	875.9	891	891.0	1970.1		<b>Kitti</b> w
Emerillon C-56	899.8	850.7	930	930.0	2368.9		Hermine E-94	863.0	765.1	889	889.0	2575.9		Heron H-73	885.0	895.6	911	911.0	2094.9		<b>Kittin</b>
Emerillon C-56	919.8	867.6	950	950.0	2374.6		Hermine E-94	883.0	780.6	909	909.0	2585.6		Heron H-73	905.0	914.7	931	931.0	2088.9		Kittiw
Emerillon C-56	939.8	884.4	970	970.0	2380.2	V1	Hermine E-94	903.0	796.0	929	929.0	2595.2		Heron H-73	925.0	934.2	951	951.0	2011.9		Kittiw
Emerillon C-56	959.8	901.5	990	990.0	2305.1		Hermine E-94	923.0	811.4	949	949.0	2604.8	2	Heron H-73	945.0	954.9	971	971.0	1851.9		Kittiw
					2000.1		///	020.0				2004.0		///	0.00.0		571	071.0			1111.

#### Figure 5: Example of computation sheet for the time calibration

	SB (mss)	1341		1st pnt ss	KB	24	dev.	SB (mss)	68		1st pnt ss	KB	24	dev.
	Albatross B-13			1625.5	shft	0		Alma F-67			400	shft	0	
	TVDss (m)	TWT cal	TWT CKS	TVD KB	MD KB	Vint		TVDss (m)	TWT cal	TWT CKS	TVD KB	MD KB	Vint	
Albatross B-13	0	0	0	24	24	1500	Alma F-67	0	0	0	24	24	1500	Annapolis
Albatross B-13	1340	1787	1787	1364	1364	1500	Alma F-67	67	89	89	91	91	1500	Annapolis
Albatross B-13	1341	1788	1788	1365	1365	1627	Alma F-67	68	91	91	92	92	1863	Annapolis
Albatross B-13	1361.0	1810.8		1385	1385	1754	Alma F-67	88.0	108.6		112	112.0	2226	Annapolis
Albatross B-13	1381.0	1833.6		1405	1405	1754	Alma F-67	108.0	126.6		132	132.0	2226	Annapolis
Albatross B-13	1401.0	1856.4		1425	1425	1754	Alma F-67	128.0	144.6		152	152.0	2226	Annapolis
Albatross B-13	1421.0	1879.2		1445	1445	1754	Alma F-67	148.0	162.5		172	172.0	2226	Annapolis
Albatross B-13	1441.0	1902.0		1465	1465	1754	Alma F-67	168.0	180.5		192	192.0	2226	Annapolis
Albatross B-13	1461.0	1924.8		1485	1485	1754	Alma F-67	188.0	198.5		212	212.0	2226	Annapolis
Albatross B-13	1481.0	1947.6		1505	1505	1754	Alma F-67	208.0	216.4		232	232.0	2226	Annapolis
Albatross B-13	1501.0	1970.4		1525	1525	1754	Alma F-67	228.0	234.4		252	252.0	2226	Annapolis
Albatross B-13	1521.0	1993.2		1545	1545	1754	Alma F-67	248.0	252.4		272	272.0	2226	Annapolis
Albatross B-13	1541.0	2016.0		1565	1565	1754	Alma F-67	268.0	270.4		292	292.0	2226	Annapolis
Albatross B-13	1561.0	2038.8		1585	1585	1754	Alma F-67	288.0	288.3		312	312.0	2226	Annapolis
Albatross B-13	1581.0	2061.6		1605	1605	1754	Alma F-67	308.0	306.3		332	332.0	2226	Annapolis
Albatross B-13	1601.0	2084.4		1625	1625	1754	Alma F-67	328.0	324.3		352	352.0	2226	Annapolis
Albatross B-13	1621.0	2107.2		1645	1645	1754	Alma F-67	348.0	342.2		372	372.0	2226	Annapolis
Albatross B-13	1641.0	2130.0		1665	1665	1754	Alma F-67	368.0	360.2		392	392.0	2226	Annapolis
Albatross B-13	1661.0	2152.8		1685	1685	1754	Alma F-67	388.0	378.2	Z1	412	412.0	2226	Annapolis
Albatross B-13	1681.0	2175.6		1705	1705	1754	Alma F-67	408.0	396.1	396.1	432	432.0	2073	Annapolis
Albatross B-13	1701.0	2198.4	Z1	1725	1725	1754	Alma F-67	428.0	417.0	417.0	452	452.0	1919	Annapolis
Albatross B-13	1721.0	2221.2	2221.2	1745	1745	2118	Alma F-67	448.0	437.8	437.8	472	472.0	1919	Annapolis
Albatross B-13	1741.0	2237.3	2237.3	1765	1765	2202	Alma F-67	468.0	458.7	458.7	492	492.0	1919	Annapolis

- The checkshot (Zss-TWT) is resampled every 20 m from Z1 (first checkshot point) to TD
- When the intersection of the well path with the main horizons will suggest a static shift value for the TZ law (an average or chosen value), the entered time shift value will:
  - statically shift the (red) TWT below Z1 ("TWT cal" column)
  - stretch the TWT values between Seabed and Z1 (purple values), giving a new constant (red) V<sub>int</sub> value in this first layer
- Such calibration will thus provide TZ and V<sub>int</sub> logs

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### **Time shift determination**

The original horizons are used to test the TZ conversion and find the best time shift (for wells with checkshot) or the shallower velocities given the best time shift (for wells with sonic) that globally adjust the converted markers with the TWT horizon intersections.

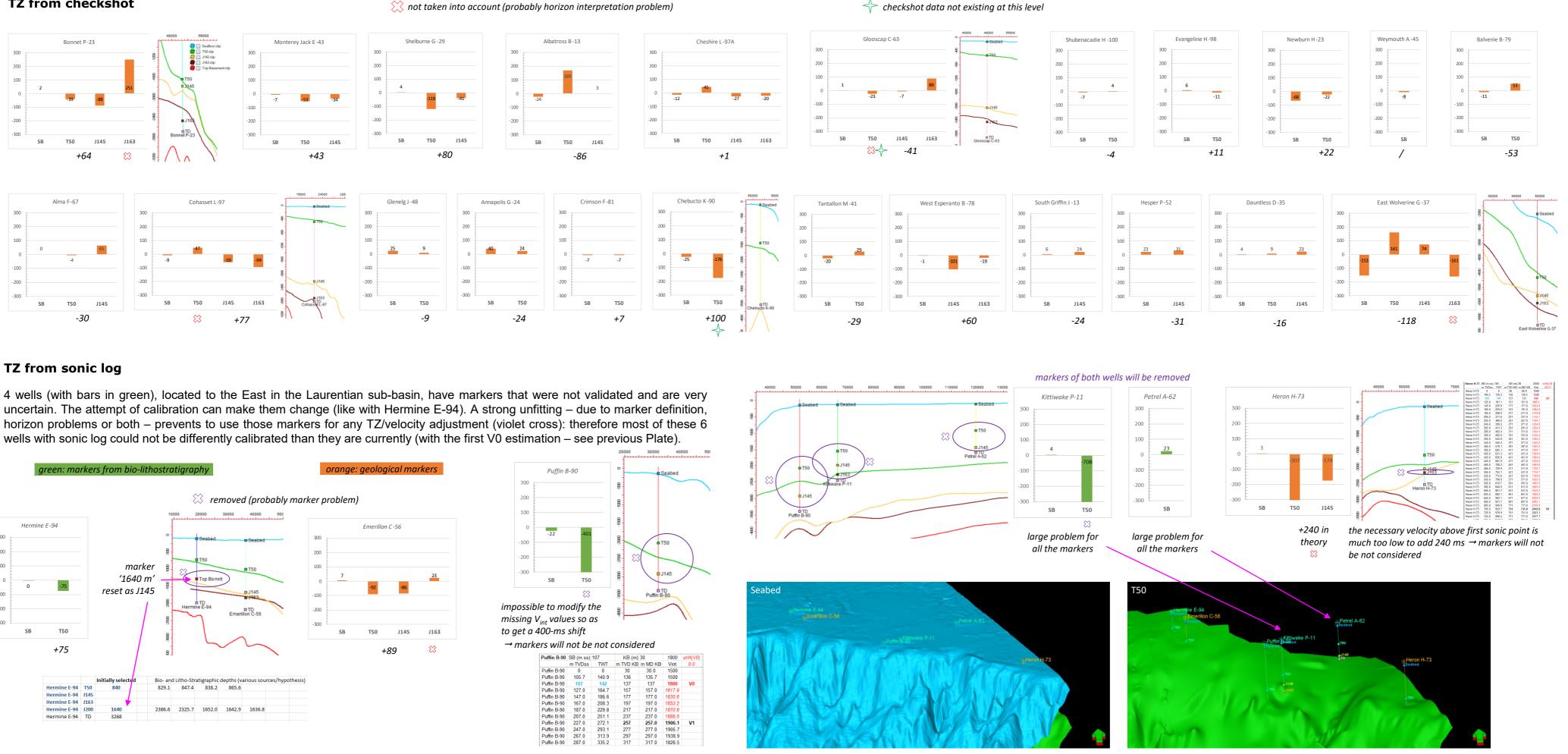
NB: concerning the checkshot calibration, it is not recommended to apply dynamical shifts (i.e. modify the whole TZ relationship to adjust all the horizon-marker correlations), only a constant static shift is searched to calibrate at best all the relevant markers. Concerning the wells with sonic, the TZ relationship computed from those sonic logs will first left as is, without any dynamic deformation, to check the degree of reliability/error in a first calibration step.

The following graphs represent the TWT error (in ms) between the well marker converted with the current TZ law and the TWT horizon intersection corresponding to that marker: error = TWT<sub>marker</sub> - TWT<sub>horizon</sub>. The wells are displayed from West (left) to East (right). The tested horizons are the original ones without editing; one must keep in mind that they are not necessarily well calibrated to their corresponding marker: they already represent merging of independent horizon grids, and the original synthetic calibrations are not available to check their geological reliability.

The number below the bars represents the selected time shift in ms (positive = downwards), which is the average on the "relevant" errors. Some markers are indeed not selected, as Seabed (SB) that will not be adjusted (error at Seabed means that the corresponding time horizon does not perfectly follow it; also the sea velocity uncertainty – set at 1500 m/s to convert the depth marker into TWT – may also add contribute to its "error"), as markers without checkshot data at their level (green cross). Some strong discrepancies are also not taken into account for the average computing (red cross) as such high value, not correctable, is probably related to horizon interpretation issues: thus, in those cases, a TWT section window comes with the bar graph to visualize the unfitting degree between the markers and the horizons.

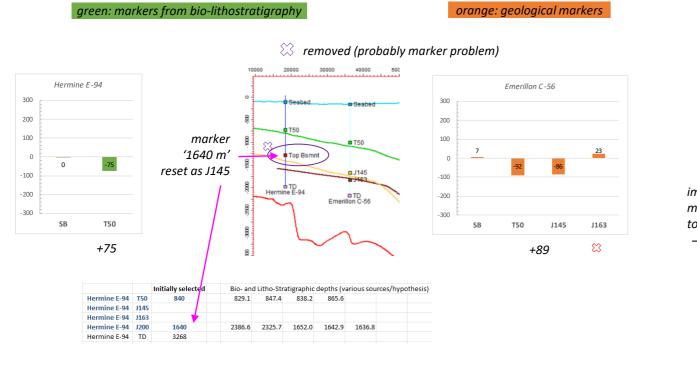
### TZ from checkshot

🔀 not taken into account (probably horizon interpretation problem)

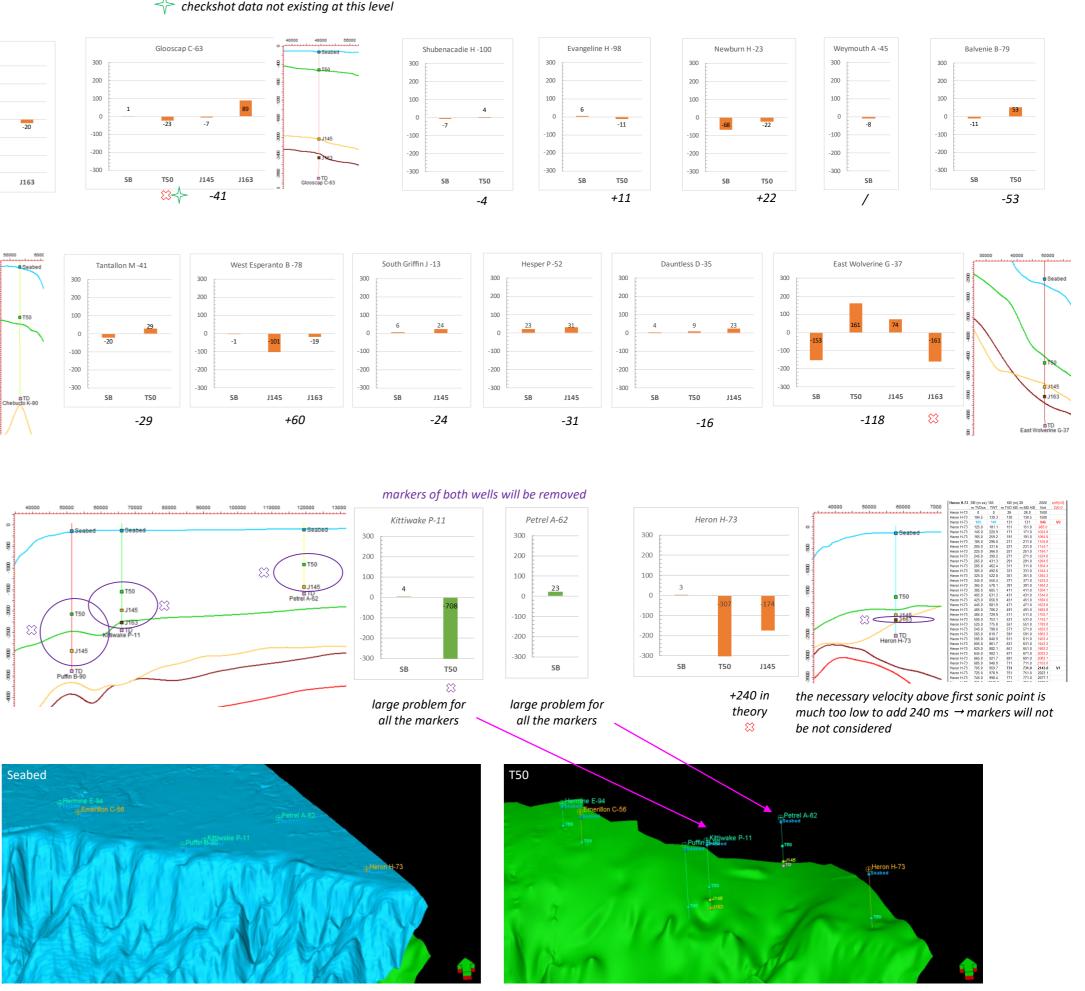


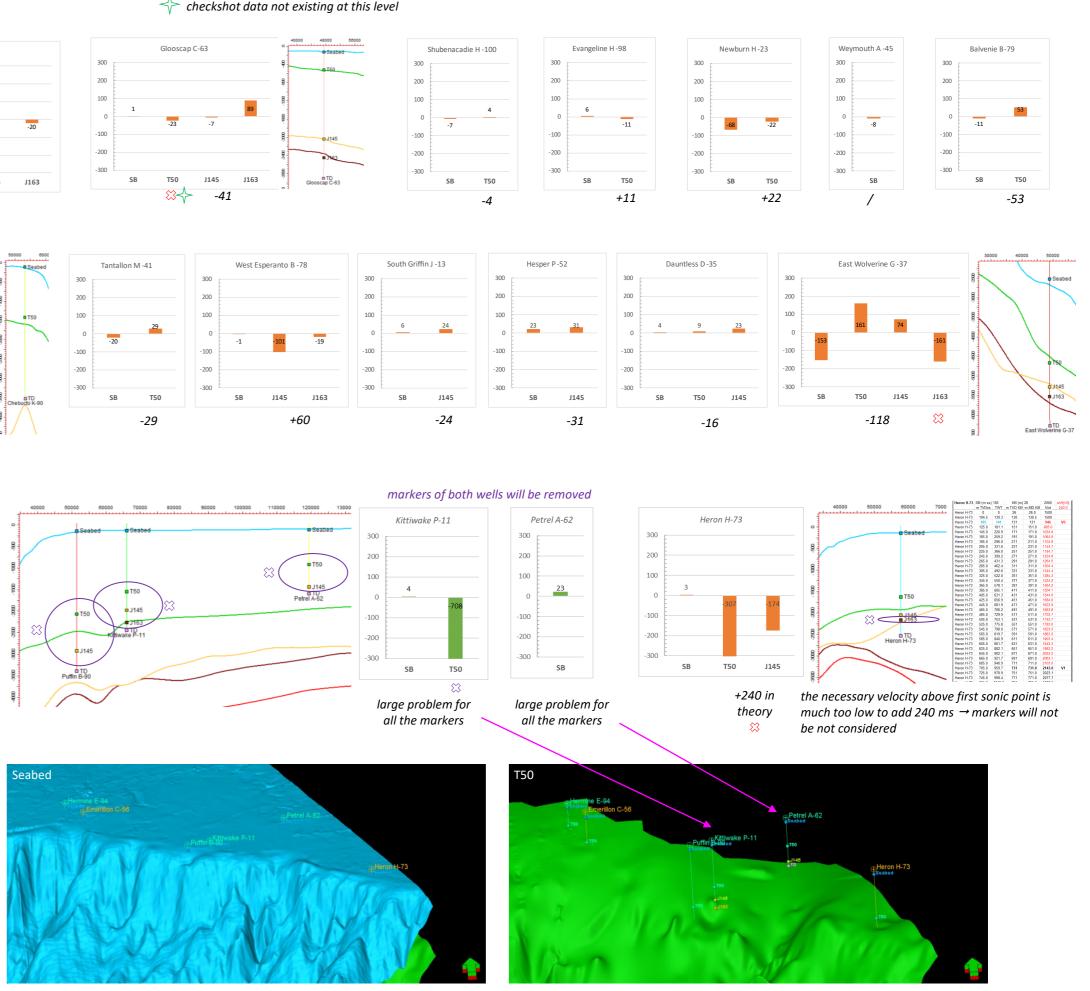
### TZ from sonic log

wells with sonic log could not be differently calibrated than they are currently (with the first V0 estimation - see previous Plate).









### Well – Time to Depth relationships (TZ) – TWT errors

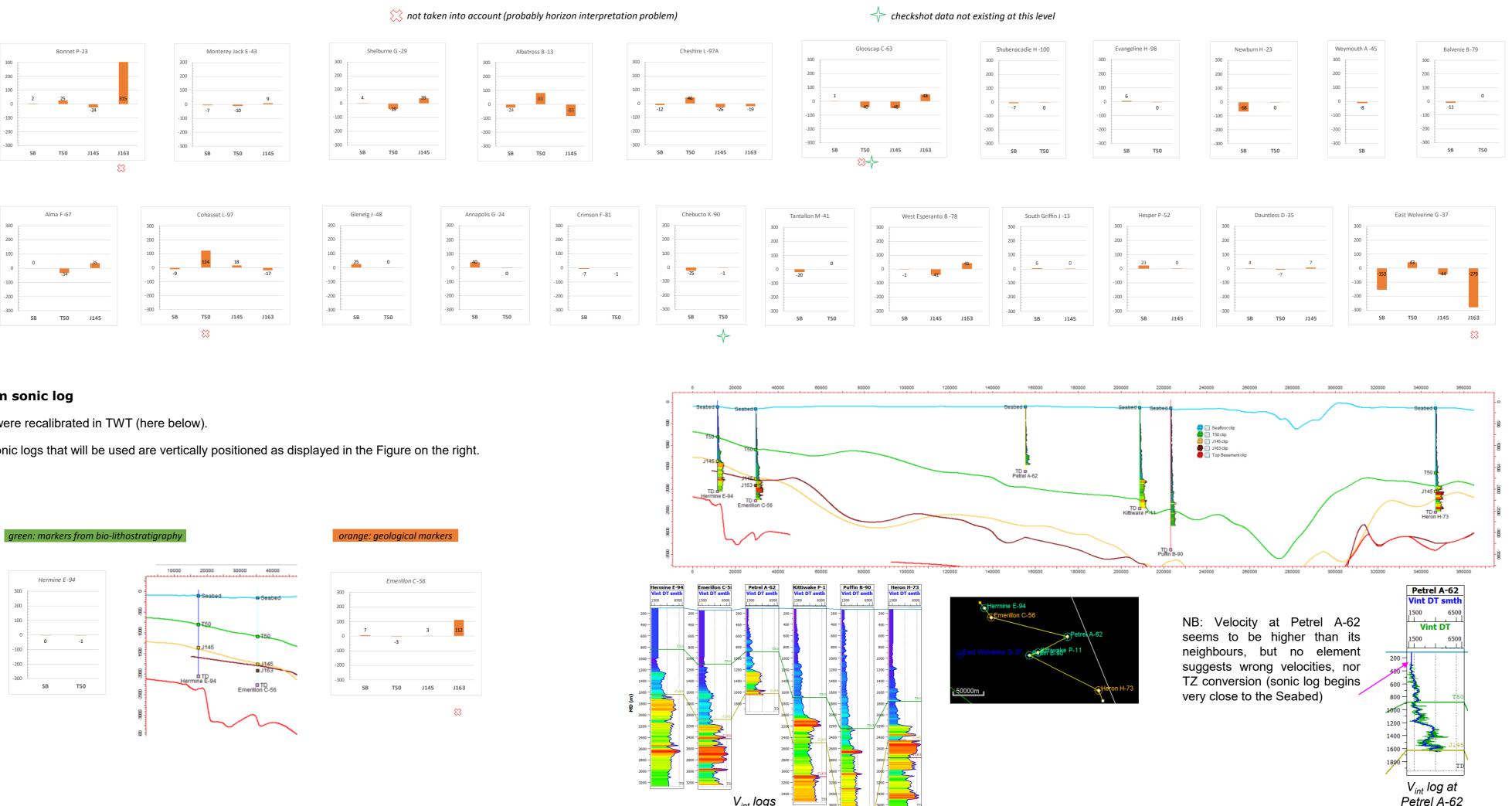
**OFFSHORE NOVA SCOTIA VELOCITY MODELING - CANADA – January 2022** 

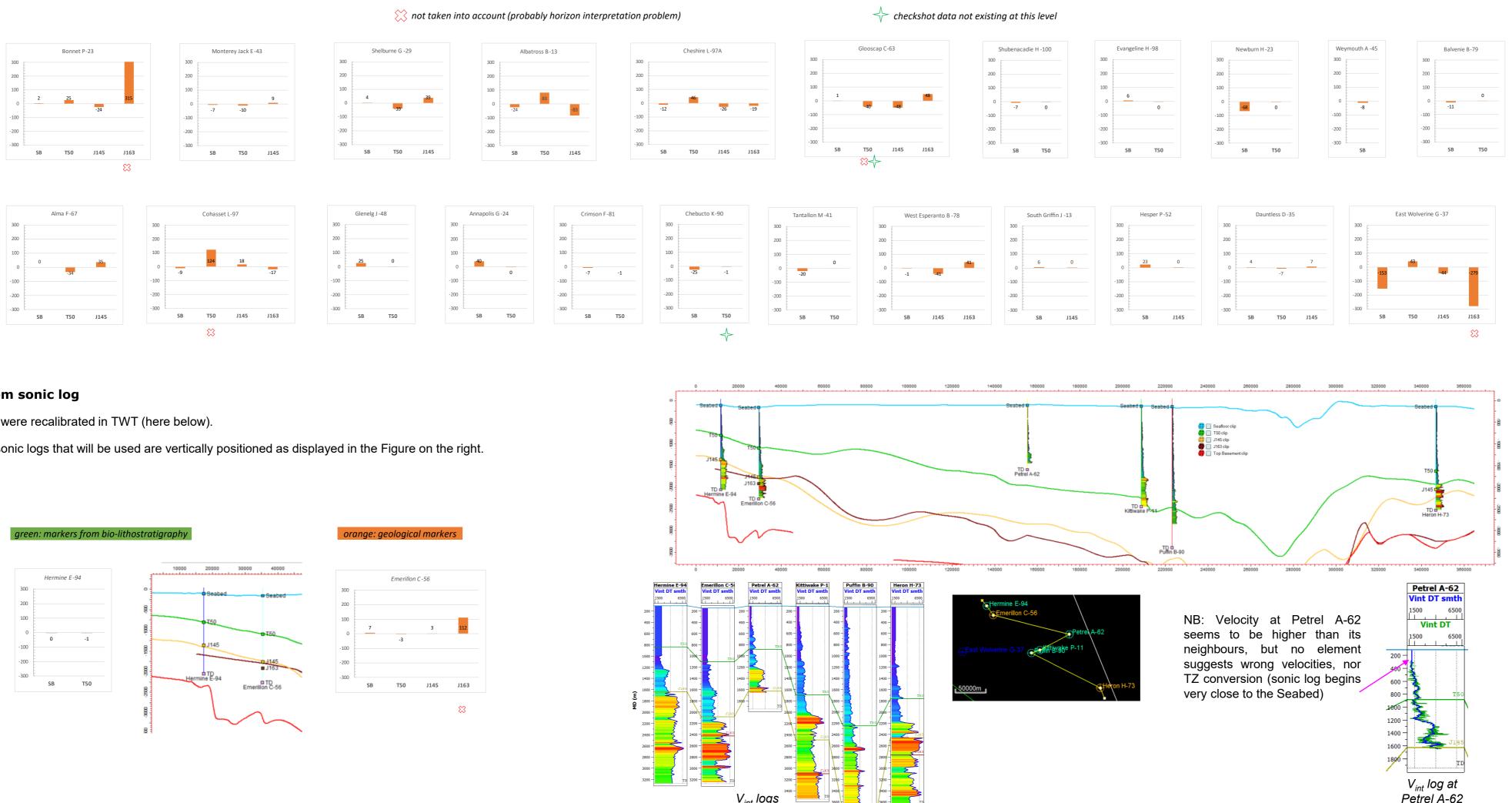
### Time shift residuals

The following graphs show what will be the expected mismatch in ms after the calibration done on:

- the wells with TZ ruled by checkshot. As no deformation of the checkshot times is possible, the final calibration is focused on the minimization of the errors on the selected/relevant markers
- the wells with recorded sonic log. Only 2 wells out of the 6 could be calibrated with the help of their markers: Hermine E-94 and Emerillon C-56. The other 4 wells could not be modified: their TZ was kept unchanged, their velocity information (sonic log) will be used in the global interpolation in the current vertical position

### TZ from checkshot

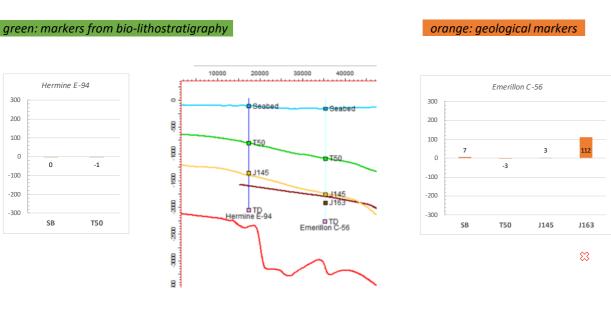


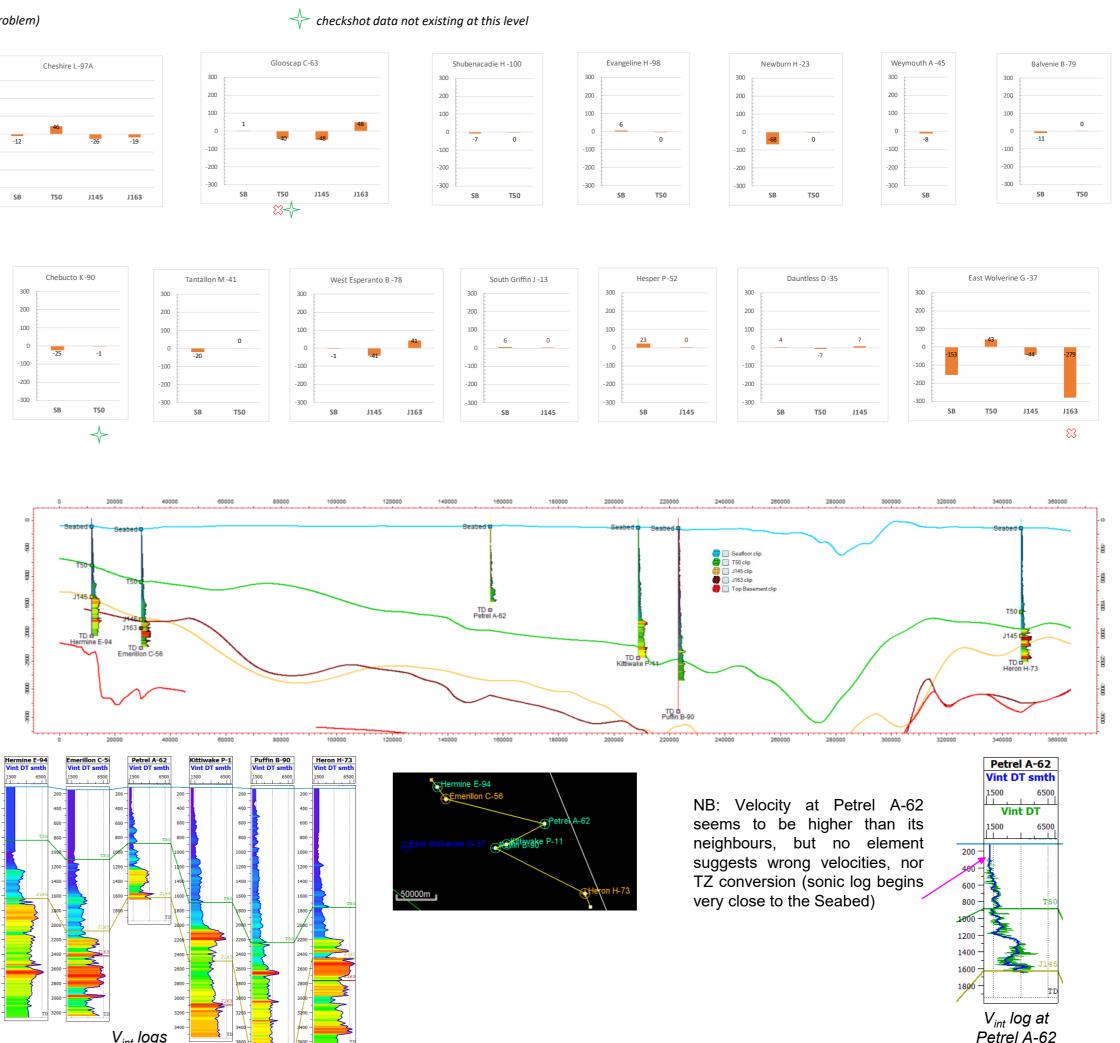


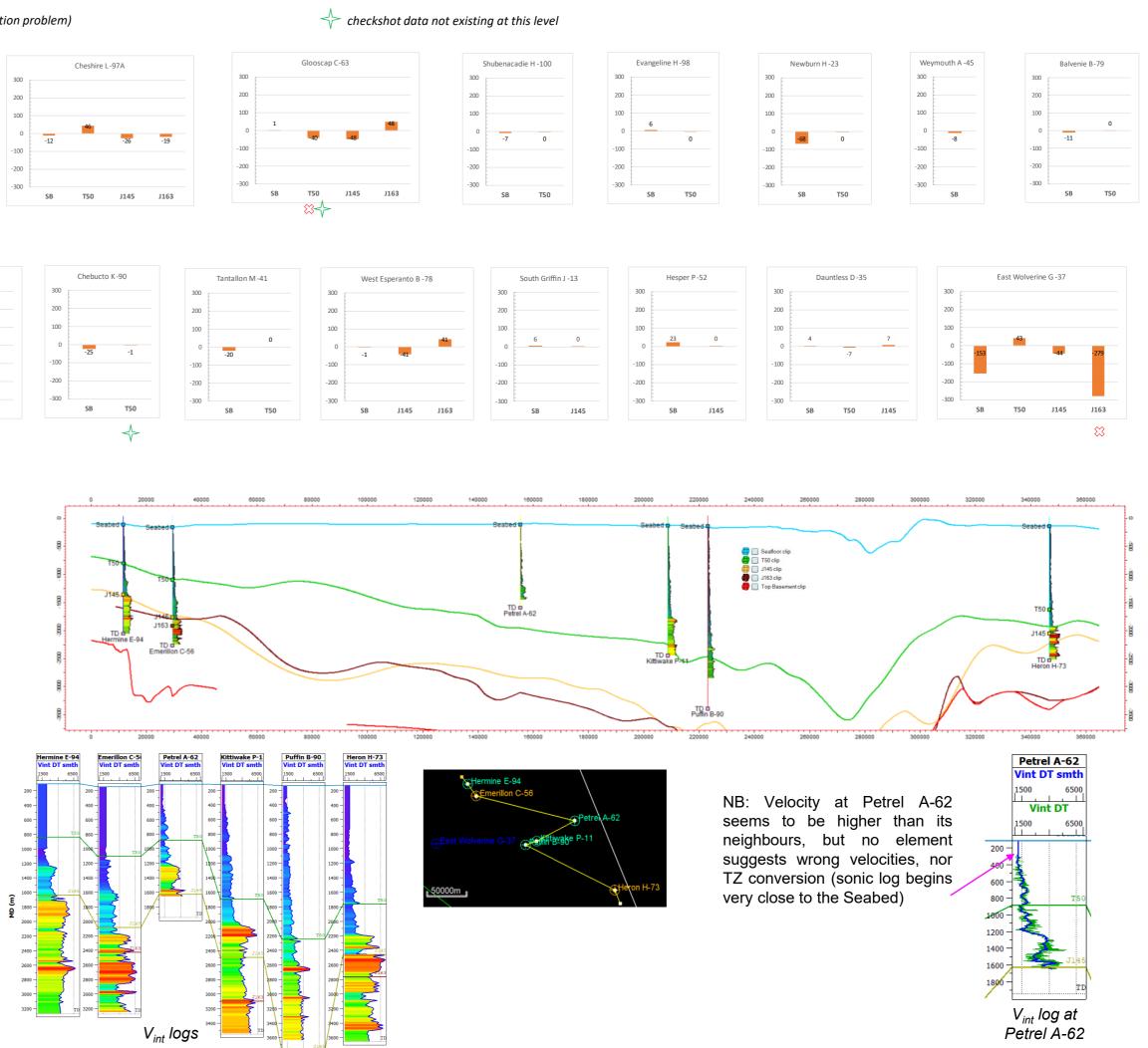
### TZ from sonic log

2 wells were recalibrated in TWT (here below).

The 6 sonic logs that will be used are vertically positioned as displayed in the Figure on the right.







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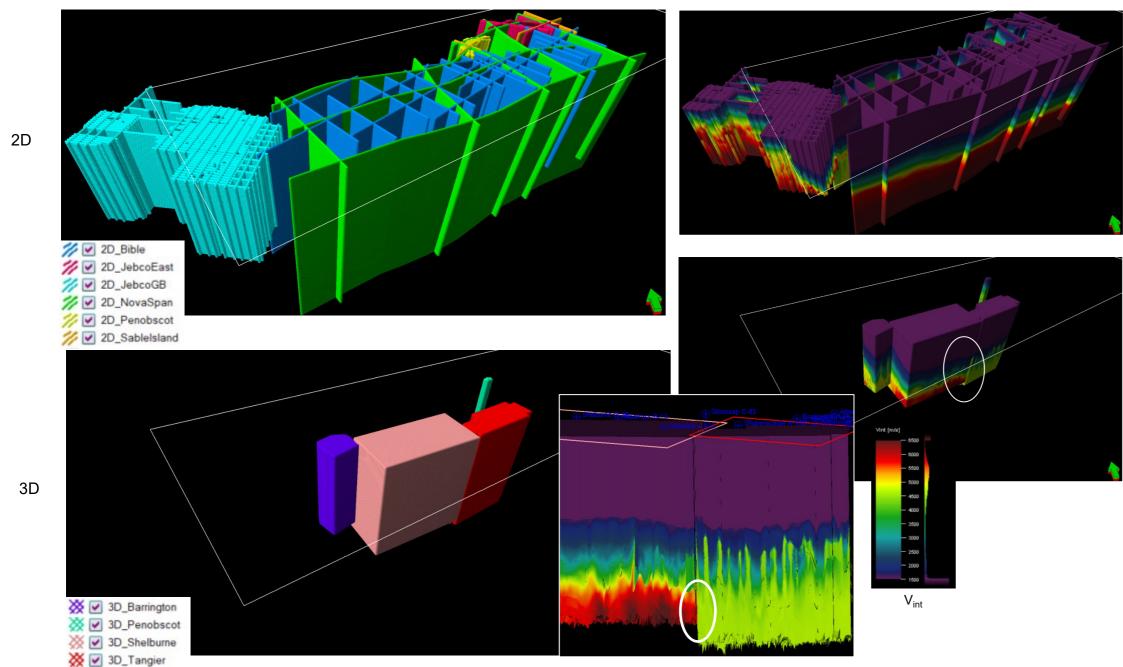
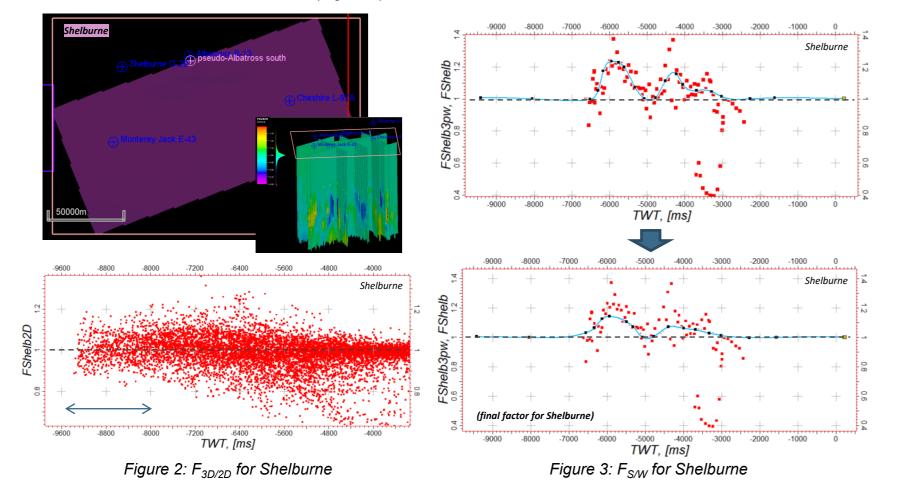


Figure 1: 2D and 3D seismic velocities and discrepancies between Shelburne and Tangier

### Shelburne

Ratio was computed with 2D velocities (Bible and Nova Span lines) and show no strong differences from 8 s to very deep levels (arrow in Figure 2). Ratio was also done with the crossing wells (to increase the number of points, the neighbouring well Albatross B-13 was laterally shifted - less than 3 km off - to get 3 intersecting wells); it gave a factor that was eventually smoothed to be held within  $\pm$  15% maximum (Figure 3).



Seismic velocities – Adjustments (1)

### Discrepancy in the seismic (processing) velocity values

Once the seismic velocities are converted in regular V<sub>int</sub>, some discrepancies appear between adjacent sources:

- between adjacent 3Ds (see white ovals at Shelburne vs. Tangier area in Figure 1)
- at 2D vs. 3D junctions

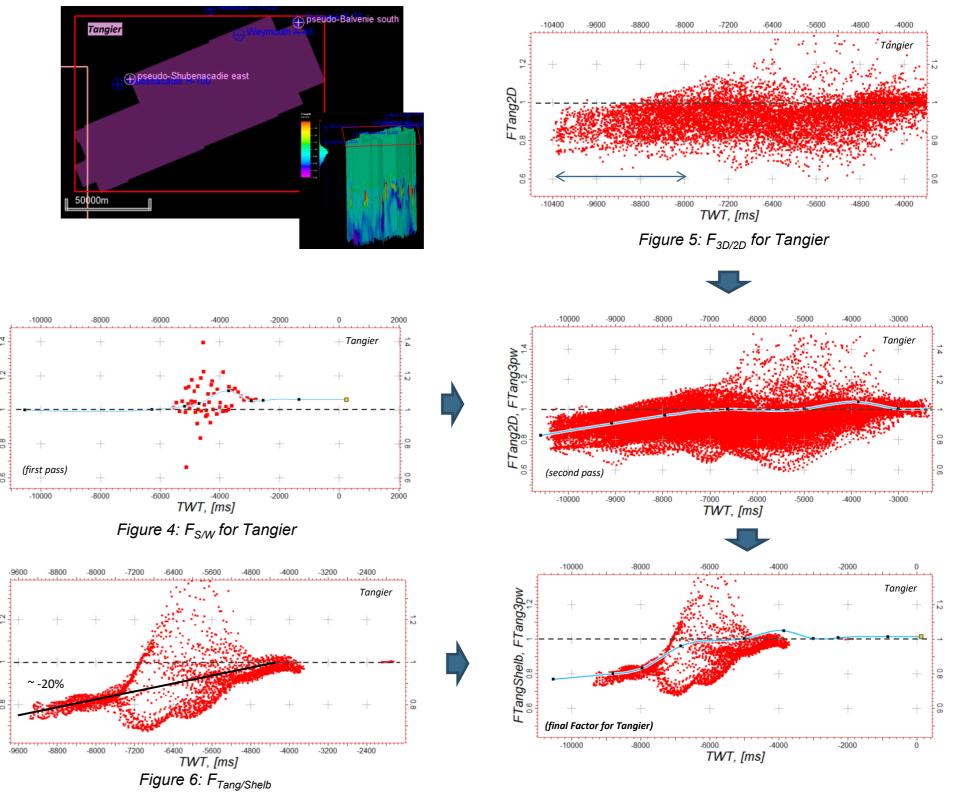
Several adjustment phases were iteratively carried out using velocity ratios (functions of TWT):

- between seismic (2D or 3D) vs. well interval velocities: F<sub>S/W</sub> = V<sub>Seis</sub> / V<sub>Well</sub>
- between 3D vs. 2D interval velocities:  $F_{3D/2D} = V_{3D} / V_{2D}$
- between two 3D interval velocities fields:  $F_{A/B} = V_{3D A} / V_{3D B}$

### Tangier

Ratio was computed with 3 wells (1 original and two laterally shifted 1.3 and 7.7 km off) but gave no clear shape (Figure 4). The comparison with 2D lines (Figure 5) show that deep Tangier velocities (> 8 s) are too slow, both analysis were used to redraw the factor considering the shallow (wells) and deep (2D) ratios.

In parallel, a ratio between Tangier and Shelburne ratios could be computed after a small lateral displacement (~2 km): the deep levels show a discrepancy of 20% (Figure 6). All the three ratios were combined to get a final ratio factor.



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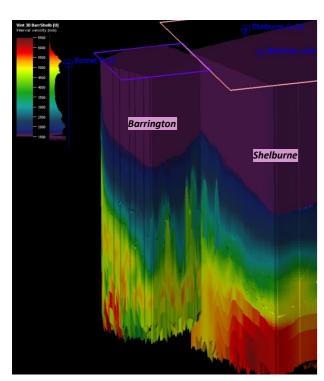


Figure 1: Discrepancies between Barrington and Shelburne cube velocities

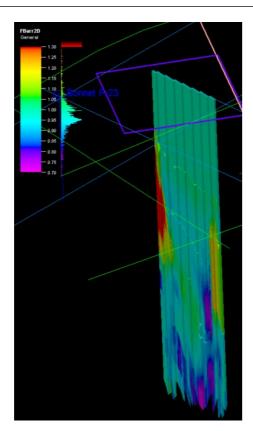
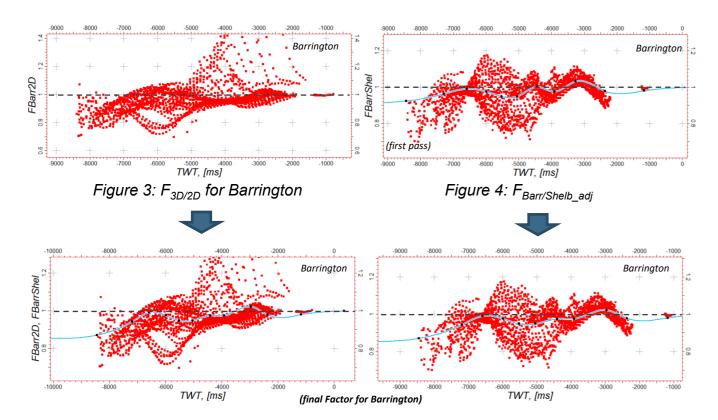


Figure 2: F<sub>3D/2D</sub> in Barrington

### Barrington

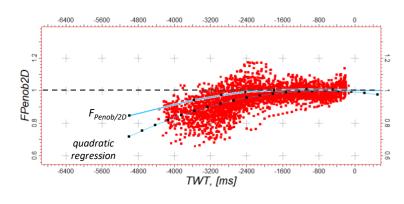
No well crosses Barrington seismic traces. Visual comparisons show small discrepancies with adjacent Shelburne velocities (Figure 1). Only one 2D lines is common with the 3D cube; a ratio factor was computed (Figure 2), showing velocities quite lower in the 3D data for the deep parts (Figure 3).

After small lateral displacement to make them overlie, a ratio was computed between both adjacent cubes (Figure 4). The ratio factor was eventually drawn to match a common shape suitable for both analysis.



### Penobscot

No well crosses Penobscot seismic traces, nor the 2D lines encompassing the 3D survey. A ratio was computed between both seismic sources (Figure 5), showing a big lowering trend in the deep parts (up to -20% - see here below).



As no other information can be extracted, the ratio factor was taken as the middle curve between the quadratic regression and the constant '1' line (see on the left).

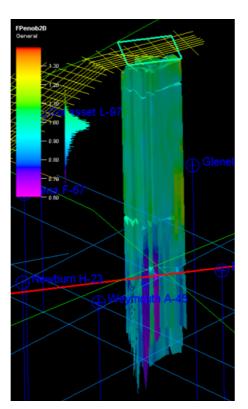


Figure 5: F<sub>3D/2D</sub> for Penobscot

<u>Wells crossing Bible lines</u>
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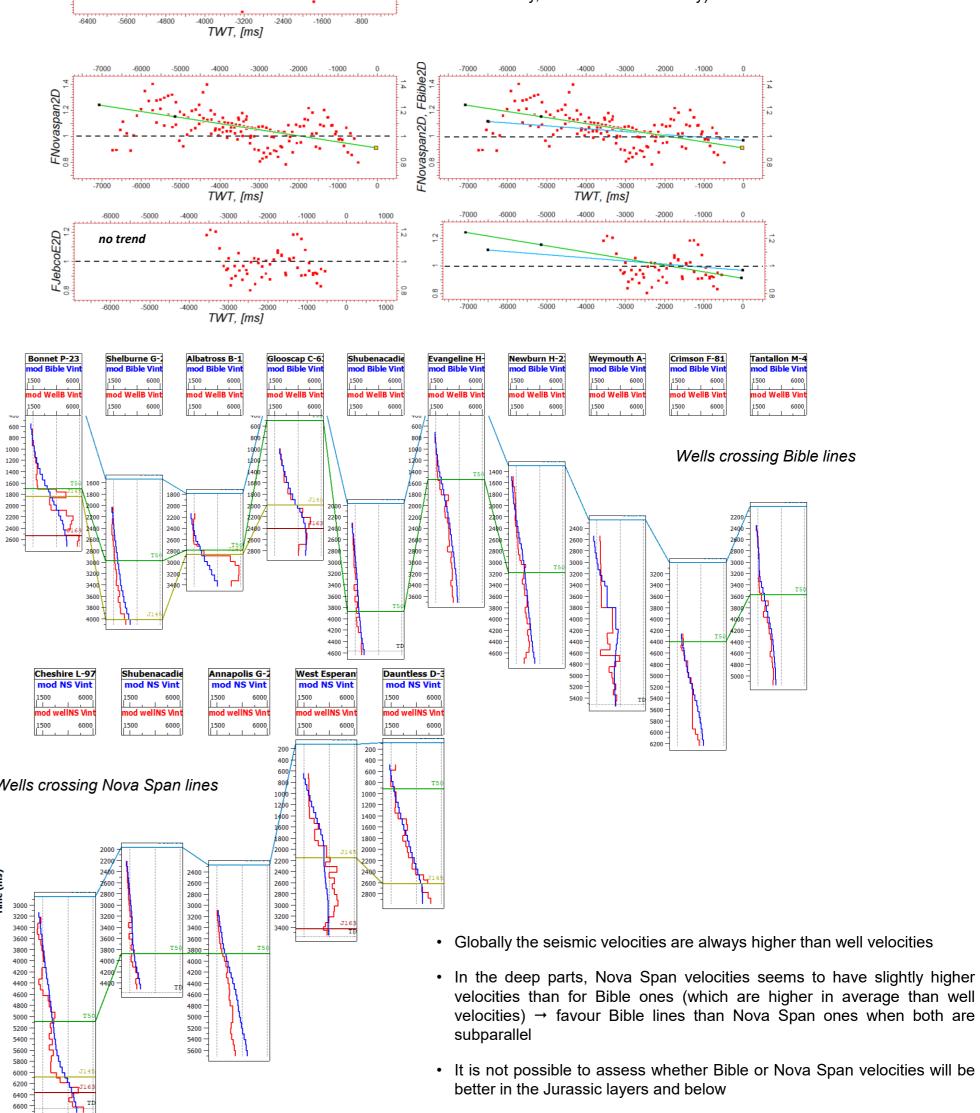
Bonnet P-23*
Shelburne G-29
Albatross B-13
Glooscap C-63
Shubenacadie H-100'
Evangeline H-98
Newburn H-23*
Weymouth A-45
Crimson F-81*
Tantallon M-41
* small shift of the well

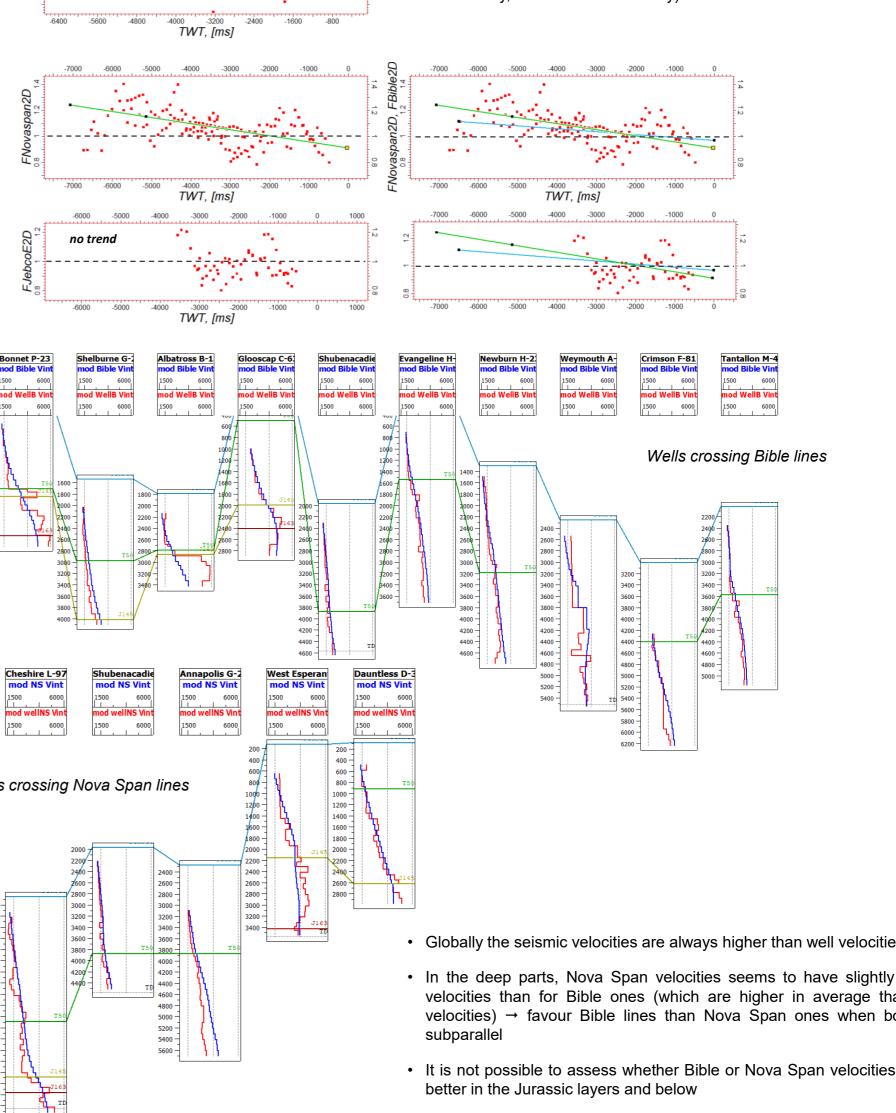
Wells crossing Nova Span lines

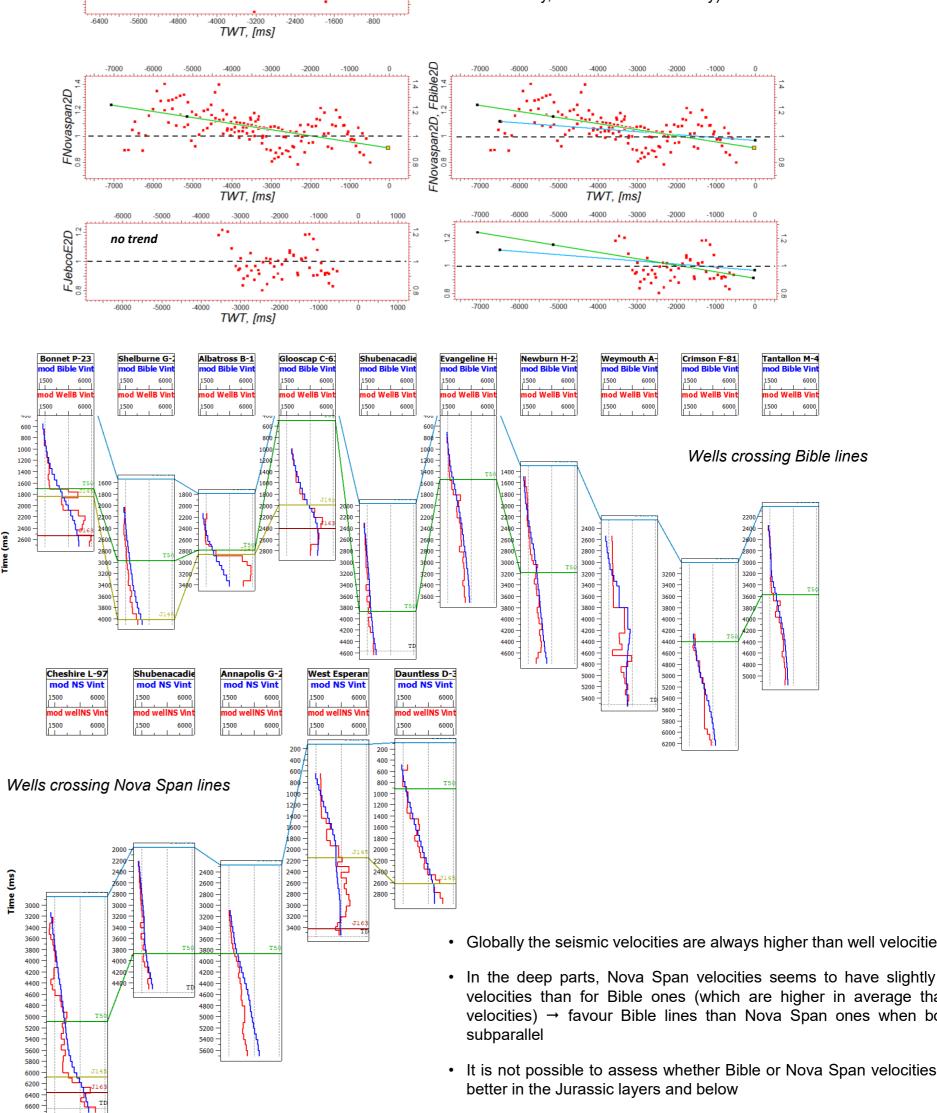
Cheshire L-97A\* Shubenacadie H-100\* Annapolis G-24 West Esperanto B-78 Dauntless D-35

Wells crossing Jebco East lines

West Esperanto B-78 Hesper P-52 South Griffin J-13









### **Bible vs. Nova Span velocities**

Bible and Nova Span lines are the most extended ones covering the main area. Nevertheless they present differences at their crossings. Velocity ratios were computed versus well velocities (see on the left with their specific linear regressions); the same work was done with the third more extended survey in the main area (Jebco East). The vertical traces in both Figures here below display the velocity traces at each well (red = well velocity, blue = seismic velocity).



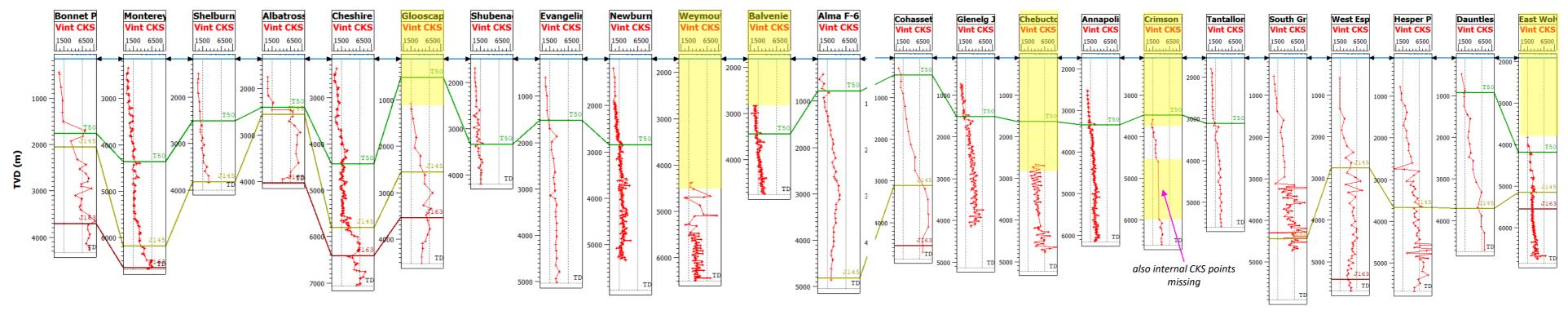


Figure 1: Wells with checkshot velocities

### Well velocities adjustment – Second pass

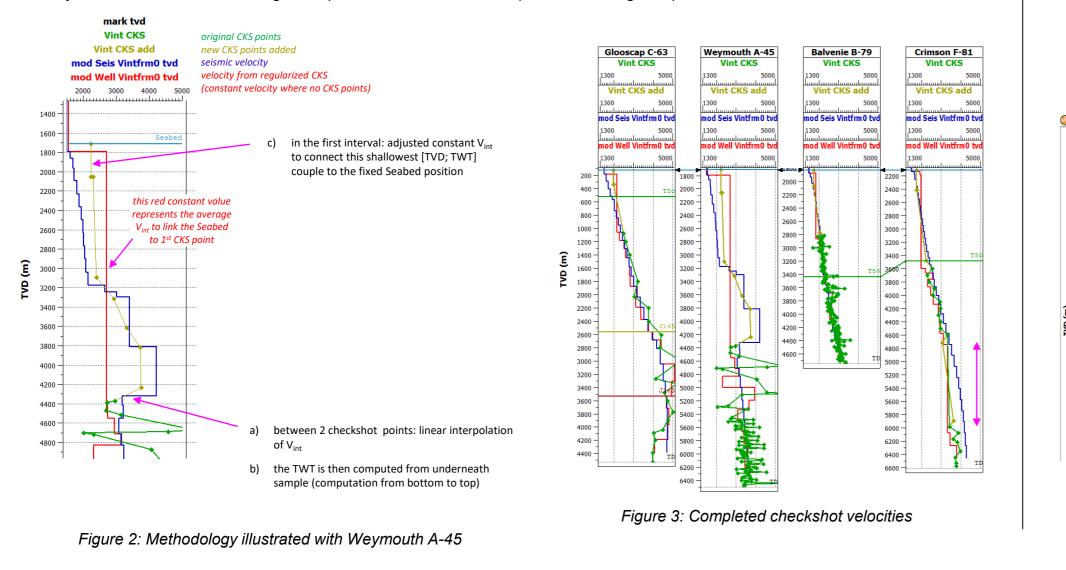
Some wells with checkshot have no data in the shallow layers (Figure 1): for Weymouth A-45 there is a gap of 2600 m between Seabed and first checkshot point. The process described in PL.2.2, is sufficiently accurate for most of the wells with checkshot (that creates constant velocity in that interval without data). The real velocity variation (~ seen by seismic velocities) would not be considered: any interpolation/co-kriging with seismic velocities would not modify it. To keep/control these shallow well velocity values (that calibrate the well in absolute) before any interpolation/co-kriging, shallow velocity points were added in these wells to follow the general seismic velocity variations. A methodology was thought to add those new [TVD; V<sub>int</sub>] couples without modifying the time-depth relationships present in the original checkshot.

6 wells were identified (see yellow parts in Figure 1). Their velocities were compared with adjacent seismic velocities, available for 4 wells among themselves (Chebucto K-90 and East Wolverine G-37 are too far from any seismic data).

The process is illustrated in Figure 2 with Weymouth A-45 example (steps in the alphabetical index 'a to c' order).

Figure 3 displays the results for the three other wells (new checkshot velocity = ocher color).

NB: all the new checkshot points are added to follow the seismic trend, and above all so that the first constant V<sub>int</sub> layer below Seabed respects a geological velocity value (higher than water velocity and lower than the following V<sub>int</sub> interval). In Crimson F-81, the interval velocity was linearized in the missing lower part of the checkshot data (see arrow in Figure 3).

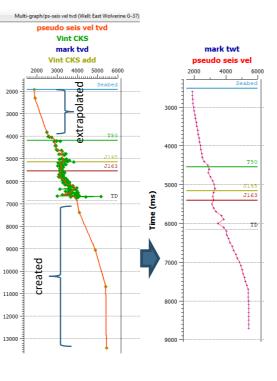


**Other velocities adjustments** 

### Velocities adjustment before gridding

Different editing was done on seismic velocities before an overall gridding:

- The adjusted 3D data were slightly cut (no overlying between different 3D)
- 2D data were cut inside 3D surveys limits (slightly extended to prevent sharp transitions)
- At 2D intersections, the lowest quality data is cut. This objective quality was defined according to their sections in PL.1.7; the order is presented in the list here below
- · When Nova Span line is subparallel to Bible one, the former is erased
- To control the extrapolation of seismic velocities eastwards (nothing in eastern third of the AOI), a pseudo seismic velocity trace is added at East Wolverine G-37, based on the well smoothed velocities (upwards, a linear extrapolation of missing velocities is applied). The resulting velocity is presented in Figure 4



1 2D\_JebcoEast 💋 🗹 2D\_JebcoGB 12 2D\_NovaSpan 💋 🗹 2D\_Penobscot 12 2D\_SableIsland choice of quality order (to prioritize the preserved data) 1. Nova Span 2. Jebco GB (1 intersection: no cut) 3. Jebco East 4. Bible 5. Sable Island 6. Penobscot (dense: no cut)

Figure 4: Pseudo seismic velocity at East Wolverine G-37

### PL. 2.7

1 2D\_Bible

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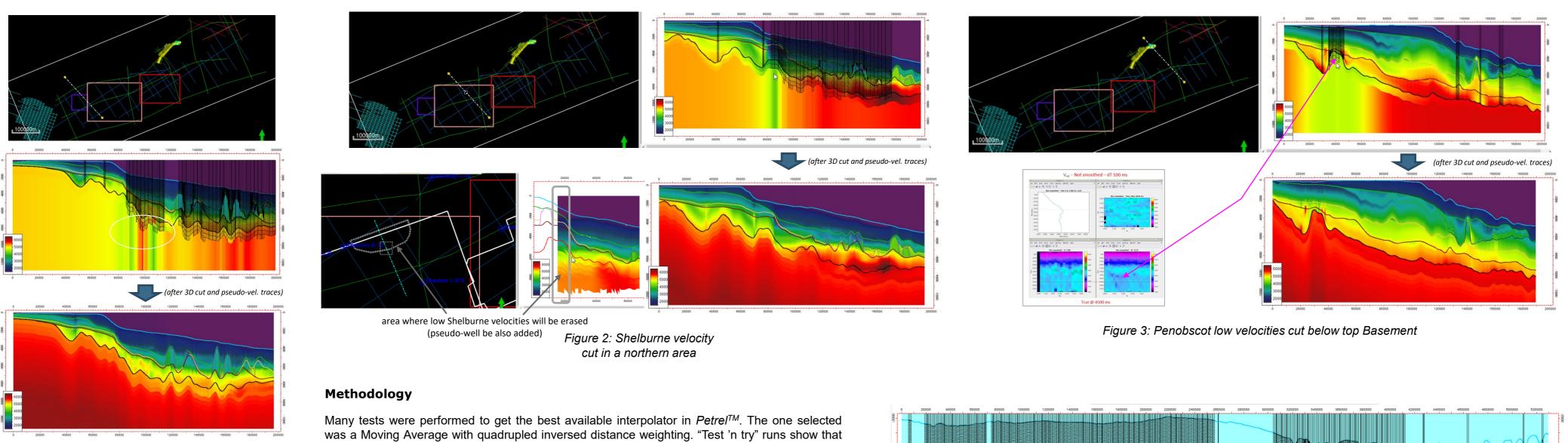
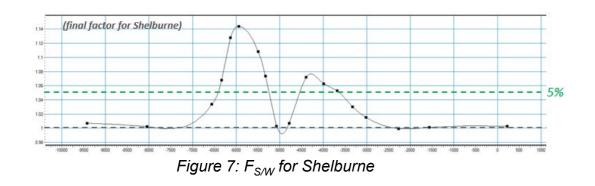


Figure 1: Barrington velocity cut below top Basement

supplementary editing passes on the seismic velocity sources were needed. They are summed up hereafter:

- All 2D data were cut below top Basement (i.e. for the incompatible Bible and Nova Span lines)
- In [top Basement; 13 s] interval, Barrington velocities are too 'chaotic' (Figure 1), which creates wrong 3D extrapolations  $\rightarrow$  velocity cut below top Basement
- Some northern Shelburne traces have low velocities (Figure 2). In this northern part, the variation of the seismic velocities field seems only horizontal: velocities can be erased without important loss of information → velocity cut below top Basement
- Penobscot velocities in [top Basement; 13 s] are manifestly too low (Figure 3); vertical sections show indeed a velocity lowering in depth → velocity cut below top Basement
- After this 3D erasing, supplementary pseudo seismic traces were added in [top Basement; 13 s] interval to help the extrapolations in the whole AOI (Figure 4): in Jebco GB survey, in the northern editing area at Shelburne, at Penobscot survey.
- After interpolation, a slight lateral smoothing filter was applied (see results in Figure 5 and 6 along a random line)
- As no well penetrates in [top Basement; 13 s] interval, no weighting adjustment could be done during a co-kriging between the secondary variable (seismic traces) and the hard data (wells). As this last interval will be defined by only seismic data, a pure assignment can be done without a well to seismic weighting. The ratio factor in Shelburne determined an average increase of 5% of the seismic velocities in the common time zone seismic vs. wells (Figure 7). Such factor of -5% was therefore applied to the seismic velocities below top Basement (see final seismic velocities in Figure 8).



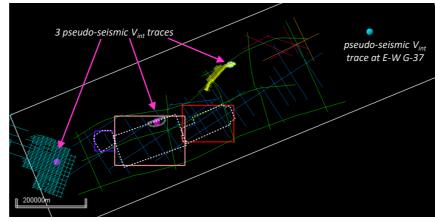
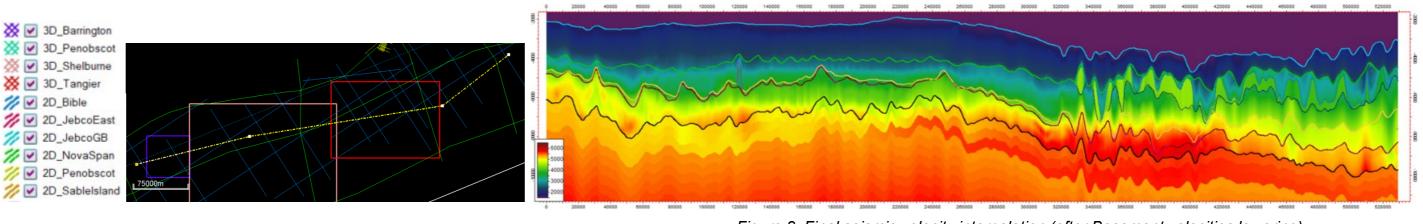
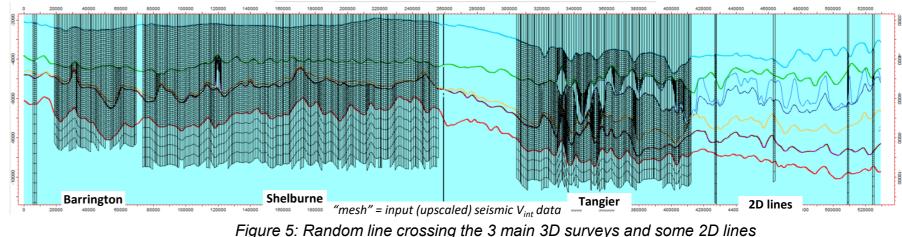
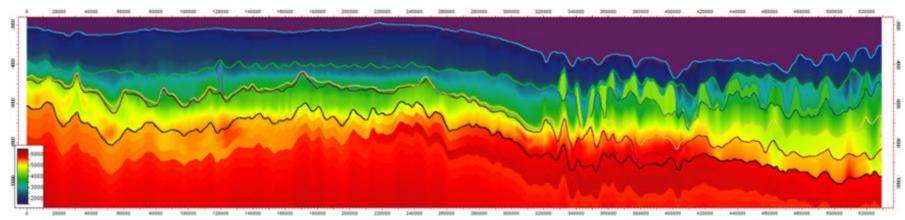


Figure 4: Pseudo seismic traces







*Figure 6: Seismic velocity interpolation after editing and smoothing* 

Figure 8: Final seismic velocity interpolation (after Basement velocities lowering)

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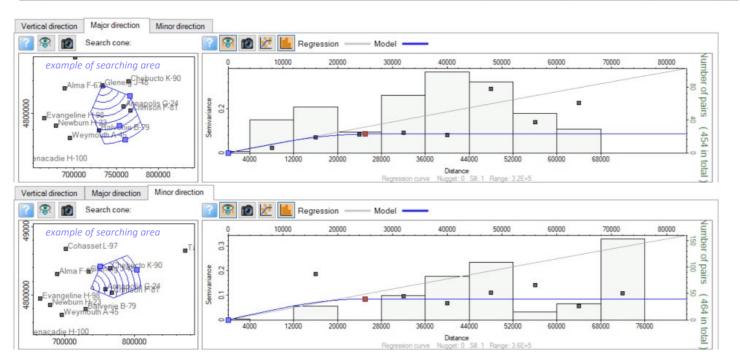
### Experimental variogram from well data

An experimental variogram from well data was computed in all the layers (parameters here below). The main results show:

- The dip direction (~N160) set as the major one gives a close range at about 25 km
- There is no real stationarity in the strike direction
- The vertical variogram is totally un-stationary (the velocity increases with depth)

Consequently, the kriging will be done with an isotropic variogram (spherical per default) with a range of 25 km.

Direction	Azimuth	Dip	Number lags	Lag distance	Search radius	Band width	Tolerance angle	Lag tolerance	Thickness
Vertical	NA	90	10	100	1000	113.6	45	50	NA
Major	158	0	9	8000	72000	25000	45	50	0.001
Minor	68	0	9	8000	72000	25000	45	50	0.001



### **Co-kriging**

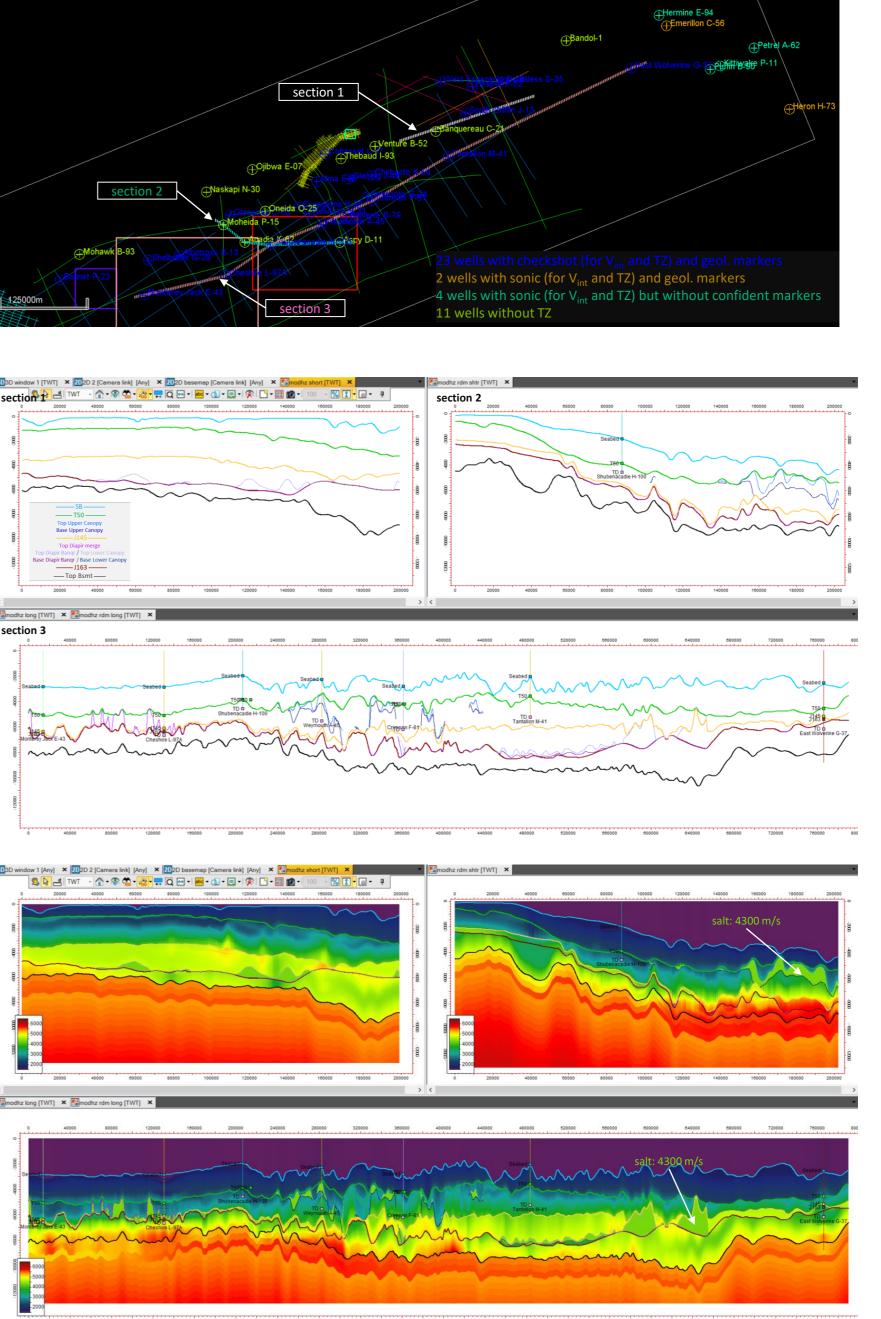
The calibrated well velocities, whether checkshot (23) or sonic velocities (6), are co-kriged with the seismic velocities as secondary variable. Some parameters are added in the following:

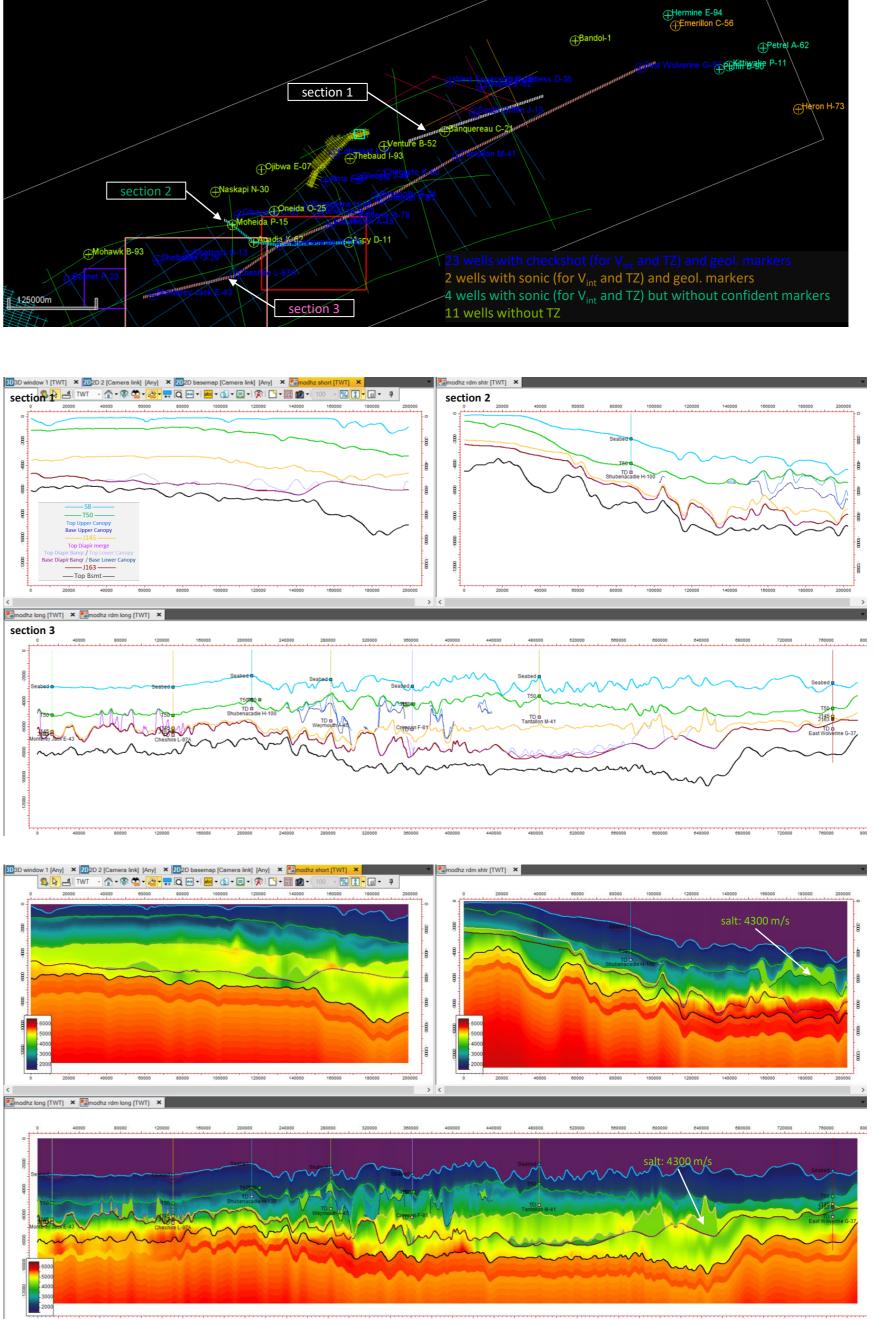
- No well enters [Top Basement; 13000 ms] interval, which prevents the whole Co-Kriging → East-Wolverine G-37 is extended to upper Basement. Nevertheless, this layer was not filled with the co-kriging results, but with the seismic velocities lowered by 5% (see previous Plate)
- The salt zones are set at 4300 m/s
- The vertical variogram is totally un-stationary (the velocity increases with depth)

A first co-kriging pass was carried out (figures presented on the right):

- Basemap showing the 3 sections (2 sections cross wells without TZ that will be incorporated furthermore)
- Sections with the all the horizons
- Result of the co-kriging

Information of the 11 remaining wells (wells without own TZ information) can be used in a second co-kriging pass: their geological markers will be converted from Depth to Time using the resulting velocities of the first pass, and those velocities will be adjusted to get a better calibration before lopping them in a last co-kriging pass.





# **CHAPTER 3**

# **DOMAIN CONVERSION**

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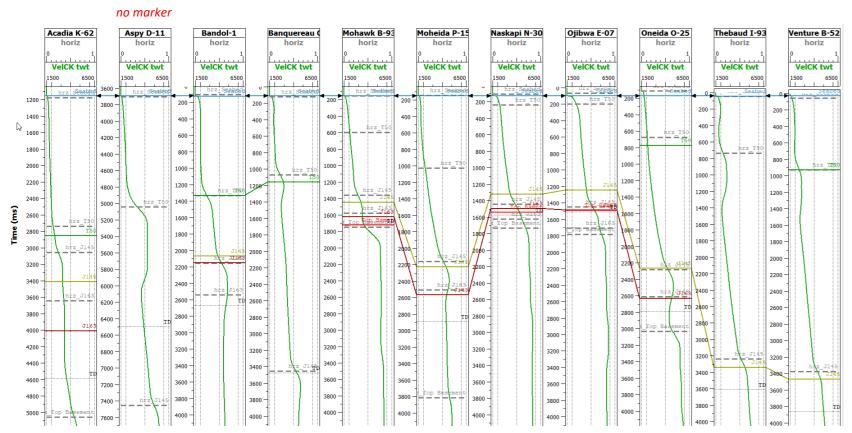


Figure 1: Velocity traces extracted at the 11 wells without own TZ

### Incorporation of wells without own TZ

After the first pass of co-kriging, the resulting velocities were extracted along the 11 remaining wells still not used (see Figure 1). These velocities were differentiated to get Depth to Time laws to convert the geological markers into TWT (markers in colors in Figure 1). The marker vertical positions can be compared with the intersections of the related TWT horizons (color in grey).

The velocities were "stretch and squeezed" in some intervals between two horizons to better fit the markers and horizons, but without necessarily reaching a "perfect match" through strongly deformed velocities from the first co-kriging results (see Figure 2). Indeed, the horizons may also be incorrect (see PL. 2.3), forcing a perfect fit through non-geological velocities is often unsuitable.

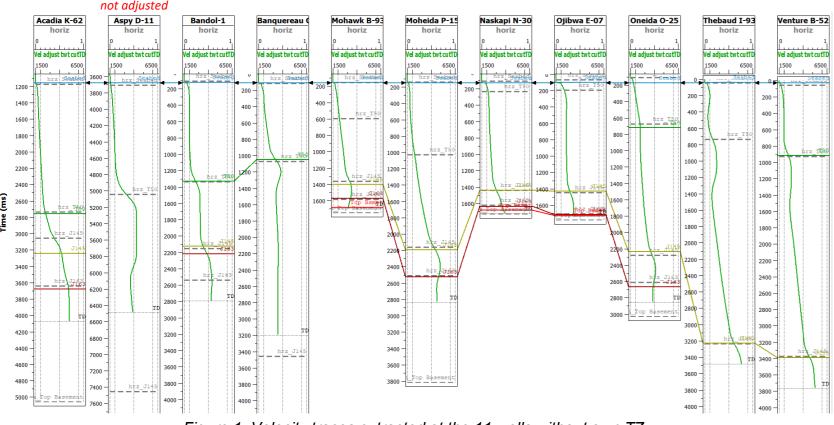
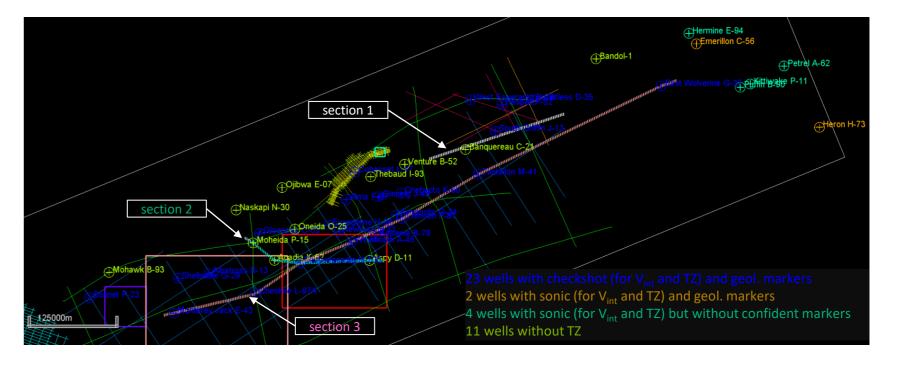


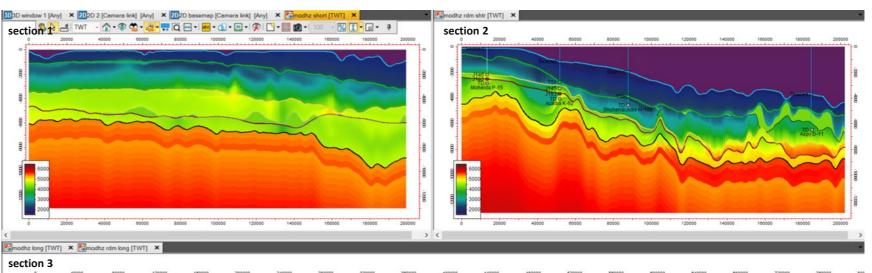
Figure 1: Velocity traces extracted at the 11 wells without own TZ

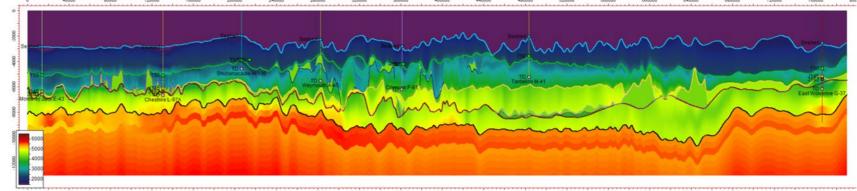
### Co-kriging with all the wells

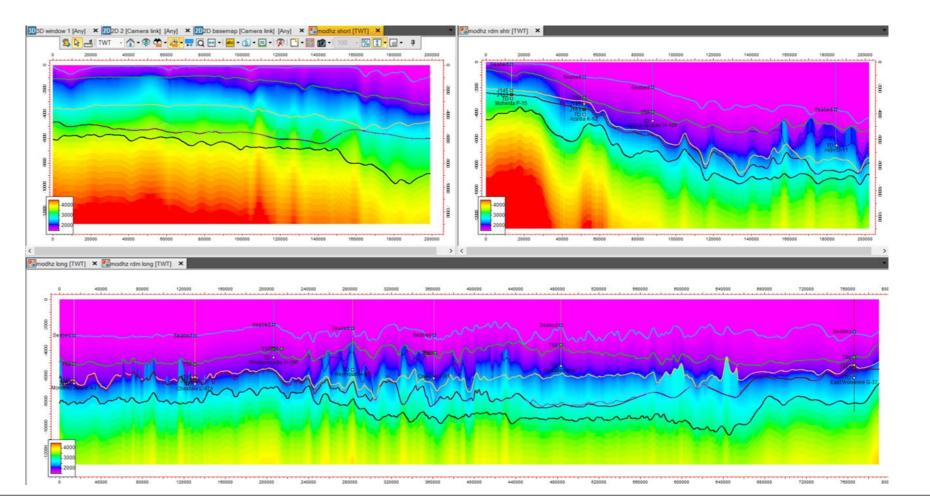
The second and final co-kriging pass was run with these 11 new wells and their adjusted velocity traces (except for Aspy D-11 without marker). The figures are presented on the right:

- Basemap showing the 3 sections
- Final V<sub>int</sub> co-kriging (some new wells without own TZ appear now on the sections)
- Conversion of V<sub>int</sub> to Average Velocity (V<sub>avg</sub>)









### **Domain Conversion**

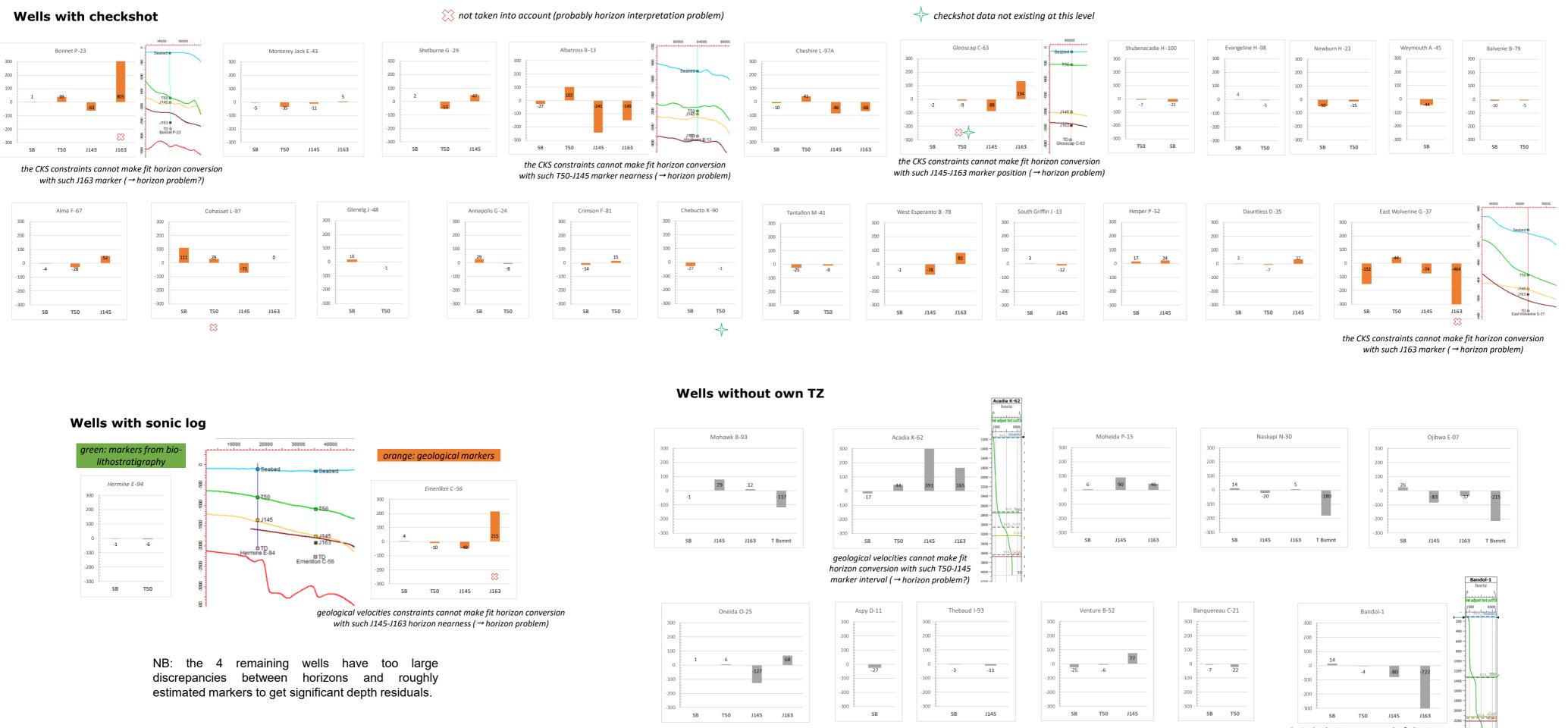
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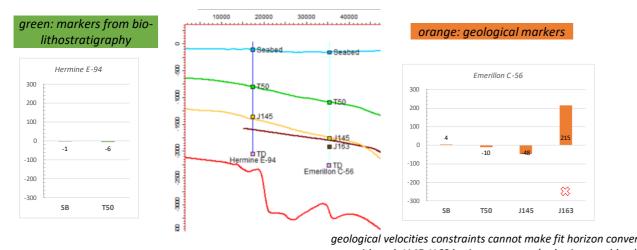
### Horizon conversion

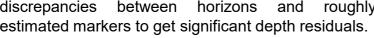
Once the Average Velocity property was implemented into *Petrel<sup>TM</sup>* Velocity Model, any TWT geological object can be converted in Time or Depth domain. The TWT horizons were converted into Depth, and their intersection compared with the related geological markers. The horizons are the original ones without editing; one must keep in mind that they are not necessarily well calibrated to their corresponding marker: they already represent merging of independent horizon grids, and the original synthetic calibrations are not available to check their geological reliability. Besides Seabed (SB) is not adjusted (discrepancy at Seabed means that its time horizon does not perfectly follow it; also the sea velocity uncertainty - set at 1500 m/s to convert the depth marker into TWT - may also add contribute to its "discrepancy").

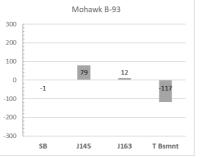
The following graphs show what is the depth mismatch in m after conversion: residual = Zss<sub>converted horizon</sub> - Zss<sub>marker</sub>. The wells are displayed from West (left) to East (right) and gathered in 3 groups:

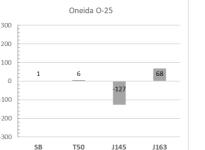
- the wells with TZ ruled by checkshot. As no deformation of the checkshot times is possible, all the horizons cannot be fitted. The strongest residuals are illustrated and commented with a TWT section
- the wells with sonic log. Plate 2.3 and -4 showed that only Hermine E-94 and Emerillon C-56 have markers coherent their related horizons (or vice versa). The depth residuals in the 4 remaining wells cannot be appraised with reliability
- the wells without any TZ recorded. As explained in the previous Plate, their fitting cannot be perfect













The adjusted velocities at these wells (from the initial co-kriging results) are sufficiently fitted: their residuals are in the same range as for wells with recorded checkshot.

# geological velocities cannot make fit horizon conversion with such J145-J163 marker nearness $(\rightarrow horizon problem?)$